

# A Comprehensive Framework for Rendering Layered Materials

EXPANDED TECHNICAL REPORT

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**Abstract:** We present a general and practical method for computing BSDFs of layered materials. Its ingredients are transport-theoretical models of isotropic or anisotropic scattering layers and smooth or rough boundaries of conductors and dielectrics. Following expansion into a directional basis that supports arbitrary composition, we are able to efficiently and accurately synthesize BSDFs for a great variety of layered structures.

Reflectance models created by our system correctly account for multiple scattering within and between layers, and in the context of a rendering system they are efficient to evaluate and support texturing and exact importance sampling. Although our approach essentially involves tabulating reflectance functions in a Fourier basis, the generated models are compact to store due to the inherent sparsity of our representation, and are accurate even for narrowly peaked functions. While methods for rendering general layered surfaces have been investigated in the past, ours is the first system that supports arbitrary layer structures while remaining both efficient and accurate.

We validate our model by comparing to measurements of real-world examples of layered materials, and we demonstrate an interactive visual design tool that enables easy exploration of the space of layered materials. We provide a fully practical, high-performance implementation in an open-source rendering system.

**Remark:** This document follows the same structure as the paper. Differences are highlighted by change bars in the right margin.

# 1 Introduction

The notion of scattering at a surface is central to rendering. It is appropriate, and computationally essential, to treat thin structures as surfaces when the scale of the scene allows: from a metal surface with microscopic imperfections to a rough ocean viewed from space, surface-scattering models are often the correct representation.

Metal or dielectric interfaces with microscopic roughness are the simplest scattering surfaces, but the vast majority of nonmetallic materials are not transparent; they reflect light diffusely by subsurface scattering. The most commonly used reflectance models, with a diffuse and a specular component, are based on the idea of a dielectric boundary above an optically dense scattering medium.

Surfaces can also be more complex, with layers that might not fully hide the material below: glaze over ceramic, wall paint over primer, colored car paint with a clear coat, vitreous enamel in gold and silver jewelry, and layered biological structures like leaves, flower petals, or skin. All these can be described in terms of a stack of layers of scattering and/or absorbing media, separated by interfaces that might be smooth or rough. At the bottom the stack could be an opaque interface (such as a metal) or a transparent one. Layers and interfaces provide a language that is useful for describing a wide range of surfaces, and which already underlies most BRDF models.

Expressing a surface explicitly as a layered system with physical parameters also allows it to be treated consistently across scales. For close views where a given structure can't be treated as a thin surface, the structure can be rendered directly, and with an accurate reduction to a surface model, it can be freely switched to a surface for farther views.

However, it is important to realize that we do not have accurate computational models for scattering from any systems more complex than a single layer or a single interface. Even the simplest nontrivial system, of a single medium bounded by a smooth interface, is only roughly approximated by standard BRDF models. Many other models have been proposed for layered or coated structures of one kind or another, but all are limited to particular special cases or lacking in terms of accuracy. Of course, it is possible to instantiate any kind of layered structure explicitly in a rendering system, relying on a general purpose rendering algorithm to resolve interactions between the layers; however, this approach is usually impractical due to the difficulty that such methods face in reliably finding light paths through a material stack.

In this paper we provide a complete solution for accurately simulating scattering from layered surfaces. Our system handles any isotropic surface that can be expressed in terms of layers and interfaces; in a sense we provide a computational language for describing surface structure. The building blocks of our system—the grammar of the language, so to speak—are basis expansions, the adding equations, and the adding/-doubling method: computational tools from radiative transport that have seen occasional use before in graphics. In this paper we develop the vocabulary needed to express the kinds of surfaces that are useful for graphics: we show how to use micro-

facet models for transmission and reflection, measured BRDFs, and media with the Henyey-Greenstein and von Mises-Fisher phase functions in this framework. We also provide efficient algorithms for evaluation and exact importance sampling at render time.

Our system is expressive but also practical. A precomputation step expands all the BSDFs and phase functions in a Fourier basis, which causes the plane-parallel multiple scattering problem to decompose into separate problems per azimuthal frequency. The multiple scattering problem is solved using adding/doubling for scattering layers and the adding equations for the sequence of layers and interfaces. Finally the resulting BSDF is stored to be used for rendering.

Our implementation scales efficiently to high orders, handling very rough to nearly mirrorlike interfaces, and isotropic to strongly peaked phase functions, while maintaining accuracy and avoiding ringing or other artifacts. The precomputed BSDF is stored in a sparse format, requiring a few kilobytes to a few megabytes, depending on the expansion order. Precomputation time is on the order of seconds, and render-time performance is close to that of dedicated implementations of BSDF models—in fact, the quality of our importance sampling technique means that precomputed representations of standard BSDF models sometimes outperform the corresponding analytic models in equal-time comparisons.

Achieving this level of accuracy and performance requires considerable care in designing representations, algorithms, and numerical techniques used in both precomputation and rendering. In this paper we discuss the design of the system and the most important issues in making it work. We will release a complete open-source implementation as part of the Mitsuba renderer [Jakob 2010].

This paper has the following contributions:

- We develop efficient and robust numerical methods for projecting a range of transport-theoretic reflectance models into a basis that supports arbitrary composition.
- We recognize the inherently sparse nature of the problem to be solved and develop a system that is able to exploit this property to scale to a wide range of layered structures including very challenging input. To our knowledge it constitutes the first practical solution for modeling the interactions of multiple rough boundaries without simplifying assumptions.
- We show how to efficiently evaluate and importance sample the resulting tabulations and propose an extrapolation method that accelerates precomputation and rendering times further when some approximations are acceptable.
- We propose a multiple scattering term for microfacet BRDFs that avoids an energy loss issue of these models.

- We develop heuristics that automatically select a basis of sufficient resolution to guarantee bounds on representation error.

## 2 Prior work

Light transport in graphics is typically done in the framework of linear transport theory (wave and quantum effects are neglected except, possibly, in deriving scattering phase functions). Predicting reflectance from layered materials at this level of accuracy is the subject of the *albedo problem* [van de Hulst 1980] in one-dimensional linear transport theory—the problem of determining the emergent distributions from plane-parallel media subject to only external sources.

Exact closed-form albedo problem solutions are rare. In graphics, Blinn [1982] used single-scattering solutions, which were extended by Hanrahan and Krueger [1993] to include index of refraction changes, multiple layers, and a Monte Carlo method for computing multiple scattering. These were some of the first graphics models to work in terms of layered media, but single-scattering solutions have limited applicability and the more general Monte Carlo method is unfortunately slow to converge—though the convergence rate can be improved in some cases by the use of scattering equations in integral form [Pharr and Hanrahan 2000]. Our work pursues the same goal with a focus on efficiency, accuracy, and generality.

Exact solutions that include all orders of scattering are limited to infinitely-thick materials with isotropic or linearly-anisotropic scattering and smooth, indexed-matched boundaries [Chandrasekhar 1960]. The semi-infinite solution for isotropic scattering involving the H-function was used by Premože [2002] to render dusty surfaces. Solutions for finite layers [Das 2010] or for semi-infinite media with Fresnel reflection [Williams 2006] require solving integral equations by iteration or other methods.

The albedo problem for a single layer with general reflecting boundary conditions has in some sense been solved exactly using either the Wiener-Hopf method [Williams 1973] or the singular eigenfunction method of Case [McCormick and Kuscer 1973]. The transport operator in plane geometry has a simple spectral expansion: the angular distribution everywhere in the layer has a unique representation as a superposition of orthogonal eigenfunctions (a separation of variables yields exponentials in optical depth multiplied by simple functions of angle  $L_\nu(z, \mu) = e^{-z/\nu} a_\nu / (2(\nu - \mu))$ ). There are a finite number of discrete eigenfunctions corresponding to rigorous diffusion, the number of which increase as the phase function becomes more peaked. However, the spectrum has a continuous component  $\nu \in [0, 1]$  and the “eigenfunctions” for this portion are singular (they include a delta-function in angle  $\mu$ ). Solving for the expansion coefficients for any particular problem and using the resulting expansion numerically is challenging in most cases [Kaper et al. 1970]. However, with carefully selected convergence acceleration schemes, these exact forms of solution can yield very accurate numerical benchmark values [Ganapol 2008].



A wide variety of approximate deterministic methods are available for computing BSDFs for general layered materials, including discrete ordinates ( $S_N$ ) [Thomas and Stamnes 2002], the transfer matrix method [Aronson 1971], the FN method [Siewert 1978], adding-doubling [van de Hulst 1980], analytical discrete ordinates [Siewert 2000], and the singular eigenfunction method [McCormick and Kuscer 1973]. These methods all have different accuracy/cost tradeoffs and stability issues [Chalhoub et al. 2003] and in principle any of them could be used to compute transport operators within our general framework.

In graphics, our approach is most similar to that of Stam [2001]. In his paper, he proposes the first BSDF model for rough dielectrics and uses it via the  $S_N$  method to compute a BSDF that models skin as an anisotropic scattering layer with rough dielectric boundaries. Our work continues in the same vein as Stam’s: we also model surfaces in terms of layers and boundaries and we work in terms of a similar directional basis. However, our system goes considerably beyond Stam’s earlier work, providing a complete, modular solution that can handle any layered structure accurately and efficiently and maintains good performance for high order expansions. This requires fundamentally different ways of computing basis expansions, representing them compactly, and solving the resulting equations robustly in the face of challenging input. Also, to the best of our knowledge, we are the first to consider importance sampling, von Mises–Fisher scattering, and an approximate multiple surface-scattering correction for rough interfaces using this approach.

Several specialized BRDF models have been proposed that approximate specific types of layered structures using coupled diffuse and specular lobes [Wolff et al. 1998; Shirley et al. 1997; Kelemen and Szirmay-Kalos 2001], including asperity scattering [Koenderink and Pont 2003], and modified microfacet distributions for rough slabs [Dai et al. 2009]. Our framework subsumes these models and is generally also more accurate as a consequence of correctly accounting for all interactions between layers. A variety of other approximate analytic methods have been proposed for rendering layered materials, such as Kubelka-Munk [Dorsey and Hanrahan 1996], diffusion-based methods [Donner and Jensen 2005], or specialized approximations for leaves [Wang et al. 2005]. A flexible family of layered BRDFs was proposed by Weidlich and Wilkie [2007]. Their approach is simple and efficient but doesn’t achieve many desirable properties that our model does, including reciprocity, energy conservation, and accurate accounting for multiple scattering within and among layers.

Neglecting polarization effects, we consider only scalar radiative transfer in this paper. Extension of our methods to handle vector radiative transfer is straightforward [Garcia 2012]. There is also the possibility of inhomogeneous scattering layers—layers where the single-scattering albedo is a function of depth, which are solvable using known methods [Yanovitskij 1997a]. Fluorescence [Wilkie et al. 2006], anomalous dispersion [Weidlich and Wilkie 2009], and thin film interference effects [Hirayama et al. 2001; Icart and Arquès 2000; Ershov et al. 2001] have been considered in re-

flectance models and could be included as components in our framework but our foremost focus here is on a comprehensive geometrical optics framework.

### 3 Background

This section describes the computational framework of our system, which builds upon a number of prior works in transport theory that we review here. We will work under a plane-parallel, or 1D transport, assumption, meaning that illumination and surface properties are assumed to be invariant across the surface, so that all functions depending on position can be modeled as depending on depth alone. Practically speaking, this means that the we are deriving a BSDF rather than a BSSRDF model.

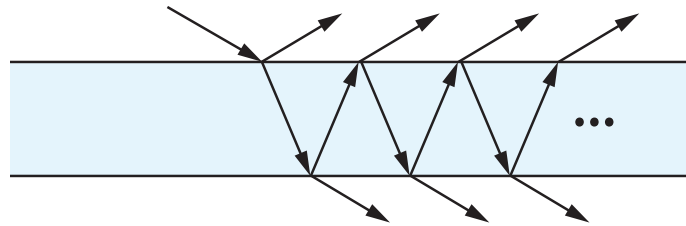
The system works in terms of radiance functions expanded in a directional basis, so that the BSDFs of layers and interfaces are represented by matrices known as *scattering matrices*.

We begin by introducing the adding equations, which are used to compute the scattering matrix of a composite layer given the scattering matrices of its constituent layers. Next, we describe the directional basis that underlies these matrix representations, and we show how to use it to discretize the radiative transfer equation and boundary conditions. Finally, we describe how to solve the radiative transfer equation using the adding-doubling method, which is named in this way due to its reliance on the adding equations to repeatedly double a layer until it has the necessary size.

#### 3.1 Adding equations

Some of the earliest theoretical work on layered materials was conducted by Stokes [1860], who analyzed the combined reflection and transmission properties of a stack of glass plates. It will be instructive to review the mathematics underlying the simplest case of his analysis involving only a single plate.

The top interface of a glass plate illuminated by a ray of unit power reflects a portion  $R$  of the light and transmits another portion  $T$  into the material, where it goes on to encounter the bottom interface, reflecting back and forth with a fraction escaping at each event:



In this case,  $R$  and  $T$  are given by the Fresnel equations. Due to reciprocity, the reflection and transmission coefficients at the bottom interface are also equal to  $R$  and

$T$ . By summing over all light paths, it is then possible to compute the total reflectance and transmittance of the plate as a whole. The resulting geometric series have a very simple explicit form:

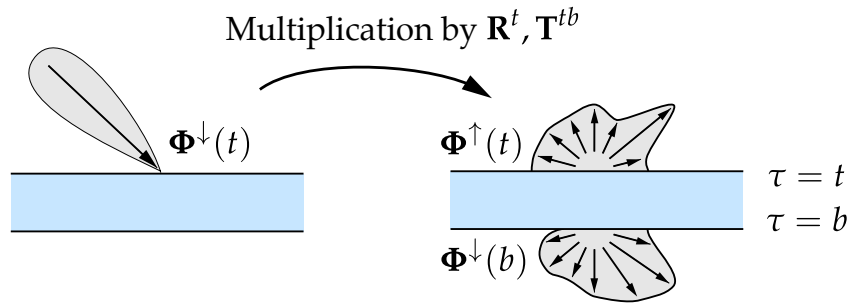
$$\begin{aligned} R_{\text{tot}} &= R + TRT + \dots = R + T^2 \sum_{i=0}^{\infty} R^{2i+1} = R + \frac{RT^2}{1 - R^2}, \\ T_{\text{tot}} &= TT + TR^2T + \dots = T^2 \sum_{i=0}^{\infty} R^{2i} = \frac{T^2}{1 - R^2}. \end{aligned} \quad (1)$$

These equations show us how to compute the scalar reflectance and transmittance of the two interfaces together from the reflectance and transmittance of the two separate interfaces.

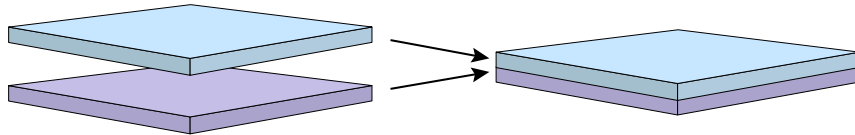
With this example in mind, let us move to a more general case: Rather than a smooth interface illuminated from a single direction, consider a slab of arbitrary composition illuminated by a radiance distribution expressed in some basis. (We leave the underlying discretization unspecified for now.) The linearity of light transport then allows us to write the scattered illumination projected into the same basis using a matrix-vector product:

$$\begin{aligned} \Phi^\uparrow(t) &= \mathbf{R}^t \Phi^\downarrow(t) + \mathbf{T}^{bt} \Phi^\uparrow(b), \\ \Phi^\downarrow(b) &= \mathbf{R}^b \Phi^\uparrow(b) + \mathbf{T}^{tb} \Phi^\downarrow(t), \end{aligned} \quad (2)$$

where  $\Phi^\uparrow(\tau)$  and  $\Phi^\downarrow(\tau)$  are vectors describing the upwards and downwards radiance at depth  $\tau$  with respect to the basis. The depths  $t$  and  $b$  correspond to the top and bottom surface, and the square matrices  $\mathbf{R}^t, \mathbf{R}^b$  and  $\mathbf{T}^{tb}, \mathbf{T}^{bt}$  describe the reflection and transmission for light arriving at the top and bottom, respectively:



The analogous question to the glass plate example is: given the scattering matrices of two distinct layers (i.e.  $\mathbf{R}_1^t, \mathbf{R}_2^t, \mathbf{T}_1^{tb}, \mathbf{T}_2^{tb}$ , etc.), what are the scattering matrices of the two layers stacked together?



Term	Meaning
$\Phi(\tau, \mu, \phi)$	Continuous radiance function
$\mu$	Cosine of the elevation angle
$\phi$	Azimuth angle
$\tau$	Optical depth within a layer
$n$	Number of discretizations in $\mu$
$m$	Number of Fourier basis functions
$\delta_{ij}$	Kronecker delta
$l$	Index used for Fourier expansions
$\alpha$	Beckmann roughness of a layer
$\sigma_t$	Extinction coefficient of a layer
$p$	Phase function of a layer
$f$	BSDF of a boundary between layers
$\Phi_l(\mu), \Phi_l$	Fourier expansion of $\phi$ and $\mu$ -discretization ( $\mathbb{R}^n$ )
$p_l(\mu, \mu'), \mathbf{P}_l$	Fourier expansion of $p$ and $\mu$ -discretization ( $\mathbb{R}^{n \times n}$ )
$f_l(\mu, \mu'), \mathbf{F}_l$	Fourier expansion of $f$ and $\mu$ -discretization ( $\mathbb{R}^{n \times n}$ )
$\mathbf{W}$	Integration weights of the quadrature scheme ( $\mathbb{R}^{n \times n}$ )

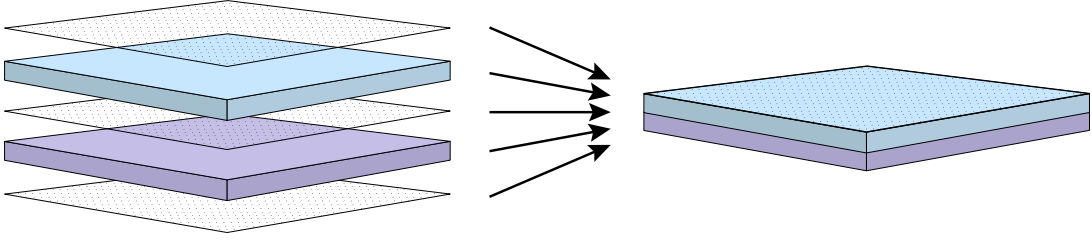
**Table 1:** Notation used in this paper

The solution is similar, but with the  $\mathbf{R}$  and  $\mathbf{T}$  matrices replacing the scalars  $R$  and  $T$ . As in the scalar case we sum over all possible sequences of reflections and transmissions, replacing geometric series by their closed-form solutions. Attention must be paid to the ordering of multiplications, since the matrices generally do not commute. For a rigorous discussion of this derivation, we refer the reader to [Grant and Hunt 1969]. The final result of this computation, analogous to (1), are the so-called *adding equations*:

$$\begin{aligned}
\tilde{\mathbf{R}}^t &= \mathbf{R}_1^t + \mathbf{T}_1^{bt} (\mathbf{I} - \mathbf{R}_2^t \mathbf{R}_1^b)^{-1} \mathbf{R}_2^t \mathbf{T}_1^{tb} \\
\tilde{\mathbf{R}}^b &= \mathbf{R}_2^b + \mathbf{T}_2^{tb} (\mathbf{I} - \mathbf{R}_1^b \mathbf{R}_2^t)^{-1} \mathbf{R}_1^b \mathbf{T}_2^{bt} \\
\tilde{\mathbf{T}}^{tb} &= \mathbf{T}_2^{tb} (\mathbf{I} - \mathbf{R}_1^b \mathbf{R}_2^t)^{-1} \mathbf{T}_1^{tb} \\
\tilde{\mathbf{T}}^{bt} &= \mathbf{T}_1^{bt} (\mathbf{I} - \mathbf{R}_2^t \mathbf{R}_1^b)^{-1} \mathbf{T}_2^{bt}
\end{aligned} \tag{3}$$

The same approach works equally well to compute the effect of a rough interface at the top or bottom of a layer or at the boundary between two layers.

The adding equations are a key ingredient of our system, since they permit accurate computation of the scattering properties of stacks of layers. We compute the scattering matrix of a layered material by repeatedly using Equation (3) to combine layers and boundaries based on a structural description of the material. This requires knowing the matrices of the interior of layers, which we discuss in Section 3.4 and of the boundaries, which is covered in Section 3.4.1.



**Figure 1:** Our framework combines interface and layer operators to form a combined material BSDF.

### 3.2 Problem statement

Before describing the basis we use to represent scattering functions and the methods used to compute the matrices used in the adding equations, we first formalize the global plane-parallel radiative transfer problem to be solved. The geometric situation is illustrated in Figure 1: we have a sequence of layers, each containing a homogeneous medium, separated by interfaces that are described by BSDFs. Because of the 1D transport assumption, the radiance depends only on direction and depth. For simplicity we define the dimensionless optical depth at  $z$ , measured from the top, as

$$\tau(z) := \int_0^z \sigma_t(z) dz \quad (\text{dimensionless})$$

where  $\sigma_t(z)$  denotes the *extinction coefficient* at depth  $z$  inside the layered material (having units of 1/distance).

Radiance is then denoted as  $\Phi(\tau, \mu, \phi)$ , where  $\mu = \cos \theta \in [-1, 1]$  is the cosine of the elevation angle, and  $\phi \in [0, 2\pi]$  is the azimuth. Using this parameterization, the radiative transport equation inside a layer takes on the following form [Chandrasekhar 1960]:

$$\mu \frac{d\Phi(\tau, \mu, \phi)}{d\tau} = -\Phi(\tau, \mu, \phi) + \int_0^{2\pi} \int_{-1}^1 \Phi(\tau, \mu', \phi') p(\mu', \phi', \mu, \phi) d\mu' d\phi', \quad (4)$$

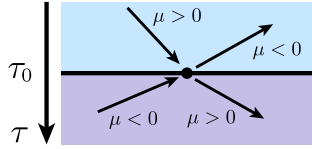
where  $p(\mu, \phi, \mu', \phi')$  is the phase function of the layer, which is a function of the angle between the directions  $(\mu, \phi)$  and  $(\mu', \phi')$ . Note that  $p$  implicitly accounts for the albedo of scattering interactions and will generally integrate to a value less than one. More formally,

$$\int_0^{2\pi} \int_{-1}^1 p(\mu', \phi', \mu, \phi) d\mu' d\phi' \leq 1 \quad \text{for all } \mu, \phi.$$

The boundary conditions of this equation are the BSDFs at the interfaces between layers. To describe interactions of light with these layer boundaries, we must distinguish between incident and exitant radiance, since a boundary at some depth  $\tau_0$

generally introduces a discontinuity in  $\Phi$ :

$$\Phi^i(\tau_0, \mu, \phi) = \begin{cases} \Phi(\tau_0^-, \mu, \phi), & \mu \geq 0 \\ \Phi(\tau_0^+, \mu, \phi), & \mu < 0 \end{cases}$$

$$\Phi^o(\tau_0, \mu, \phi) = \begin{cases} \Phi(\tau_0^+, \mu, \phi), & \mu \geq 0 \\ \Phi(\tau_0^-, \mu, \phi), & \mu < 0 \end{cases}$$


With these definitions, the surface illumination integral at a layer boundary (accounting for both reflection and transmission) takes the form:

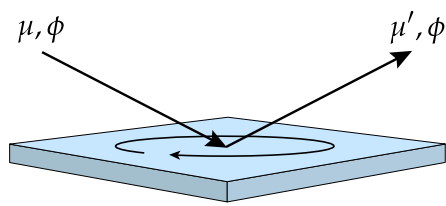
$$\Phi^o(\tau_0, \mu, \phi) = \int_0^{2\pi} \int_{-1}^1 \Phi^i(\tau_0, \mu', \phi') f(\mu', \phi', \mu, \phi) |\mu| d\mu' d\phi', \quad (5)$$

where  $f$  is the BSDF of the boundary.

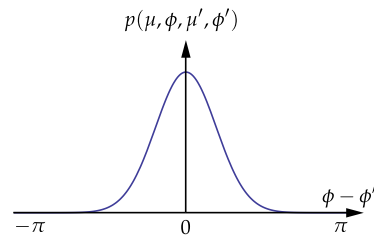
### 3.3 Directional basis

Before we can proceed to use the adding equations to solve actual problems, we must decide on a basis that is used to represent the space of radiance functions. To discretize  $\Phi$  in direction, we rely on a basis originally proposed by Chandrasekhar [1960]. It represents the light distribution at depth  $\tau$  using a Fourier series in the azimuth angle  $\phi$  and point samples in the elevation angle cosines  $\mu$ . In this section, we review this representation and motivate its choice. After projection onto this space, the radiative transfer equation and surface illumination equations also take on different forms, which we derive for completeness.

We restrict our analysis to surfaces that are isotropic, in the sense of invariance with rotation around the normal (a), and add the further reasonable assumption of bilateral symmetry (b):



(a) Isotropy



(b) Bilateral symmetry

Together these imply that all relevant quantities only depend on  $\mu$ ,  $\mu'$ , and  $|\phi - \phi'|$ .

There are two types of scattering functions that are used as inputs to our system: phase functions characterizing the optical behavior of scattering layers, as well as BSDFs characterizing interactions with layer boundaries. We represent both with even real Fourier expansions with respect to  $\phi - \phi'$  and point sample them in the  $\mu$  argument.

We now derive this representation step by step, starting with the azimuthal dependence. For a phase function  $p(\mu, \phi, \mu', \phi')$ , we set

$$p(\mu, \phi, \mu', \phi') = \sum_{l=0}^{\infty} p_l(\mu, \mu') \cos(l(\phi - \phi')) \quad (6)$$

where  $p_l(\mu, \mu')$  denotes the  $l$ -th Fourier coefficient of  $p$  as a function of azimuth for fixed  $\mu$  and  $\mu'$ . In practice, the series terms greatly decrease in magnitude as  $l \rightarrow \infty$  so that (6) can be truncated after some maximum index  $m$  where the terms have become sufficiently small. This is dictated by the lowest frequency integrand—for a e.g. diffuse layer only the  $l = 0$  term is necessary regardless of the frequency of the illumination.

This is the key benefit of the Fourier expansion—the problem of computing radiance as a function of  $\mu$ ,  $\mu'$ , and  $\phi - \phi'$  has been reduced to a series of *separate* problems each involving only  $\mu$  and  $\mu'$ . In practice, the coefficients  $p_l$  and  $f_l$  decay rapidly as  $l \rightarrow \infty$  so that only problems up to some maximum index  $m$  need to be solved. The value of  $m$  dictated by the highest azimuthal frequency that could be created in a reflection or transmission of sharp illumination. For a diffuse layer, the reflection is always constant in azimuth, and hence only the  $l = 0$  term is necessary.

Fourier series are often treated with reluctance when dealing with functions that may contain narrow peaks, but they offer important benefits in this case: the separation into independent problems for each azimuthal mode significantly reduces the difficulty of the problem that must be solved. This is a consequence of the convolution theorem, which is unique to the Fourier family of basis functions. By taking advantage of inherent symmetries in the underlying scattering functions, their dimension is furthermore reduced from 4D to 3D. As we will see later, in conjunction with sparsity, these properties will allow us to go to high order expansions to represent even mirror-like reflectors accurately. Finally, projecting existing material models onto this space involves a sequence of one-dimensional integrals, which can be evaluated cheaply using recurrences (details in Section 5). Our system could in principle also be realized using other types of basis functions, but this would involve complications due to the loss of at least one of the above properties.

### Projection of the radiative transfer equation

Having projected the phase function onto a directional representation, we can now apply the same modification to the rest of the radiative transfer equation. Note that, for an even real  $2\pi$ -periodic function  $g(\phi)$ , the  $l$ -th Fourier coefficient can be extracted by means of the following integral (where  $\delta_{ij}$  refers to the Kronecker delta)

$$\mathcal{F}_l[g] := \frac{2 - \delta_{0l}}{\pi} \int_0^\pi g(\phi) \cos(l\phi) d\phi, \quad (7)$$

such that

$$g(\phi) = \sum_{l=0}^{\infty} \mathcal{F}_l[g] \cos(l\phi).$$

Since an isotropic material is completely defined by its response to incident illumination that is even with respect to azimuth  $\phi$ , we can assume without loss of generality that the radiance function  $\Phi$  is also given by an even real Fourier series such that

$$\Phi(\tau, \mu, \phi) = \sum_{l=0}^{\infty} \Phi_l(\tau, \mu) \cos l\phi.$$

Note that it is fine to expand the illumination in a basis that is too smooth to represent it; in this setting, the BSDF frequency content is the decisive factor.

Recall the definition of the radiative transfer equation (4):

$$\mu \frac{d\Phi(\tau, \mu, \phi)}{d\tau} = -\Phi(\tau, \mu, \phi) + \int_0^{2\pi} \int_{-1}^1 \Phi(\tau, \mu', \phi') p(\mu', \phi', \mu, \phi) d\mu' d\phi',$$

The projection of the first two terms is simply

$$\mathcal{F}_l \left[ \mu \frac{d\Phi(\tau, \mu, \phi)}{d\tau} \right] = \mu \frac{d\Phi_l(\tau, \mu)}{d\tau} \quad (8)$$

$$\mathcal{F}_l [-\Phi(\tau, \mu, \phi)] = -\Phi_l(\tau, \mu) \quad (9)$$

For the last term, we first insert the definitions of  $\Phi$  and  $p$  in terms of Fourier series and integrate over  $\phi'$ , which yields

$$\begin{aligned} & \int_0^{2\pi} \int_{-1}^1 \Phi(\tau, \mu', \phi') p(\mu', \phi', \mu, \phi) d\mu' d\phi' \\ &= \sum_{l_1, l_2=0}^{\infty} \int_{-1}^1 \Phi_{l_1}(\tau, \mu') p_{l_2}(\mu', \mu) \int_0^{2\pi} \cos(l_1 \phi') \cos(l_2(\phi' - \phi)) d\phi' d\mu' \\ &= \sum_{l_1, l_2=0}^{\infty} \int_{-1}^1 \Phi_{l_1}(\tau, \mu') p_{l_2}(\mu', \mu) (\pi \delta_{l_1 l_2} (\cos(l_1 \phi) + \delta_{0l_1})) d\mu' \\ &= \sum_{k=0}^{\infty} \int_{-1}^1 \Phi_k(\tau, \mu') p_k(\mu', \mu) (\pi (\cos(k\phi) + \delta_{0k})) d\mu' \end{aligned}$$

The Fourier projection of this expression then results in

$$\begin{aligned} & \mathcal{F}_l \left[ \sum_{k=0}^{\infty} \int_{-1}^1 \Phi_k(\tau, \mu') p_k(\mu', \mu) (\pi (\cos k\phi + \delta_{0k})) d\mu' \right] \\ &= \frac{2 - \delta_{0l}}{\pi} \int_0^{\pi} \cos(l\phi) \left[ \sum_{k=0}^{\infty} \int_{-1}^1 \Phi_k(\tau, \mu') p_k(\mu', \mu) (\pi (\cos k\phi + \delta_{0k})) d\mu' \right] d\phi \\ &= \pi(1 + \delta_{0l}) \int_{-1}^1 \Phi_l(\tau, \mu') p_l(\mu', \mu) d\mu' \quad (10) \end{aligned}$$

After putting the terms (8), (9), and (10) back together, we obtain an infinite sequence of projected radiance transfer equations.

$$\mu \frac{d\Phi_l(\tau, \mu)}{d\tau} = -\Phi_l(\tau, \mu) + \pi(1 + \delta_{0l}) \int_{-1}^1 \Phi_l(\tau, \mu') p_l(\mu', \mu) d\mu' \quad (l = 0, \dots, \infty) \quad (11)$$



Note that the  $l$ –th equation only involves the  $l$ –th Fourier coefficients of the radiance field and phase function, since the azimuth and elevation dependence of the problem fully decouples in frequency space. The main consequence of this separation is that our system has to solve a number of independent subproblems over elevation angles alone. The number of problems that must be solved is related to the highest azimuthal frequency content present in  $p$ .

### Projection of the surface illumination equation

To describe interactions of light with layer boundaries, we project the surface illumination equation in much the same way. For this, note that a boundary at some depth  $\tau_0$  generally introduces a discontinuity in  $\Phi$  so that we must distinguish between the radiance just above and below it—or, more conveniently, the incident and exitant radiance, which are defined as

$$\Phi^i(\tau_0, \mu, \phi) = \begin{cases} \Phi(\tau_0^-, \mu, \phi), & \mu \geq 0 \\ \Phi(\tau_0^+, \mu, \phi), & \mu < 0 \end{cases} \quad \text{and} \quad \Phi^o(\tau_0, \mu, \phi) = \begin{cases} \Phi(\tau_0^+, \mu, \phi), & \mu \geq 0 \\ \Phi(\tau_0^-, \mu, \phi), & \mu < 0 \end{cases}$$

With these definitions, the integral takes on the following form:

$$\Phi^o(\tau_0, \mu, \phi) = \int_0^{2\pi} \int_{-1}^1 \Phi^i(\tau_0, \mu', \phi') f(\mu', \phi', \mu, \phi) |\mu'| d\mu' d\phi'.$$

where  $f$  is the BSDF of the boundary. Analogously to the medium case, we can now make use the isotropy and evenness of the BSDF to replace  $f$ , as well as the incident and exitant radiance functions,  $\Phi^i$  and  $\Phi^o$ , by even real Fourier expansions such that

$$\begin{aligned} f(\mu, \phi, \mu', \phi') &= \sum_{l=0}^{\infty} f_l(\mu, \mu') \cos(l(\phi - \phi')), \\ \Phi^i(\tau_0, \mu, \phi) &= \sum_{l=0}^{\infty} \Phi_l^i(\mu) \cos(l\phi), \\ \Phi^o(\tau_0, \mu, \phi) &= \sum_{l=0}^{\infty} \Phi_l^o(\mu) \cos(l\phi). \end{aligned}$$

Using a computation analogous to that in (10), we obtain an infinite sequence of projected surface illumination equations, one for each Fourier mode.

$$\Phi_l^o(\mu) = \pi(1 + \delta_{0l}) \int_{-1}^1 \Phi_l^i(\mu') f_l(\mu', \mu) |\mu'| d\mu' \quad (l = 0, \dots, \infty) \quad (12)$$

As before, this will later result in a number of independent subproblems, the size of which is related to the highest azimuthal frequency content present in  $f$ .

### 3.3.1 Discretization over elevation angles

We now turn to the  $\mu$  dependence: here, a quadrature scheme with integration nodes  $\{\mu_1, \dots, \mu_n\} \subset [-1, 1] \setminus \{0\}$  and weights  $\{w_1, \dots, w_n\}$  is used to discretize the integration variable  $\mu'$ . This turns the Fourier-space surface illumination integral (12) into a sum:

$$\Phi_l^o(\mu) = \pi(1 + \delta_{0l}) \sum_{i=1}^n w_i \Phi_l^i(\mu_i) f_l(\mu_i, \mu) |\mu_i| \quad (13)$$

To write out discretized forms of the radiative transfer and surface illumination equations, it will be convenient to introduce the following notation:

$$\begin{aligned} \Phi_l(\tau) &:= (\Phi_l(\tau, \mu_k))_k \in \mathbb{R}^n & \mathbf{P}_l &:= (p_l(\mu_i, \mu_j))_{ij} \in \mathbb{R}^{n \times n} \\ \Phi_l^i(\tau) &:= (\Phi_l^i(\tau, \mu_k))_k \in \mathbb{R}^n & \mathbf{F}_l &:= (f_l(\mu_i, \mu_j))_{ij} \in \mathbb{R}^{n \times n} \\ \Phi_l^o(\tau) &:= (\Phi_l^o(\tau, \mu_k))_k \in \mathbb{R}^n & \mathbf{W} &:= (\delta_{ij} w_i)_{ij} \in \mathbb{R}^{n \times n} \\ \mathbf{M} &:= (\delta_{ij} \mu_i)_{ij} \in \mathbb{R}^{n \times n} & \bar{\mathbf{M}} &:= (\delta_{ij} |\mu_i|)_{ij} \in \mathbb{R}^{n \times n} \end{aligned}$$

The discrete analogue of Equation (11) is then given by

$$\begin{aligned} \mu \frac{d\Phi_l(\tau, \mu_i)}{d\tau} &= -\Phi_l(\tau, \mu_i) + \pi(1 + \delta_{0l}) \int_{-1}^1 p_l(\mu', \mu_i) \Phi_l(\tau, \mu') d\mu' \\ &\approx -\Phi_l(\tau, \mu_i) + \pi(1 + \delta_{0l}) \sum_{i=1}^n p_l(\mu_j, \mu_i) w_i \Phi_l(\tau, \mu_i) \quad (l = 0 \dots, \infty) \end{aligned}$$

or, using matrix and vector notation,

$$\mathbf{M} \frac{d\Phi_l(\tau)}{d\tau} = -\Phi_l(\tau) + \pi(1 + \delta_{0l}) \mathbf{P}_l \mathbf{W} \Phi_l(\tau). \quad (l = 0 \dots, \infty) \quad (14)$$

Similarly, the surface illumination equation turns into

$$\Phi_l^o(\tau_0) = \pi(1 + \delta_{0l}) \mathbf{F}_l' \mathbf{W} \bar{\mathbf{M}} \Phi_l^i(\tau_0). \quad (l = 0 \dots, \infty) \quad (15)$$

Complexity-wise, it is worth noting that with this representation, a radiance distribution has size  $m \times n$ , a scattering function has size  $m \times n \times n$ , and the cost of transforming one by the other is  $m \times n^2$  (i.e. not  $(mn)^2$ ).

A wide range of quadrature schemes are applicable in this setting; in our implementation, we use Gauss-Lobatto points [Chandrasekhar 1960], which include the endpoints  $\pm 1$  and maximize the order of exactly integrable polynomials subject to this constraint.

## 3.4 Solving for the scattering matrices

Recall that in our system, we plan to use the adding equations (Section 3.1), whose input are scattering matrices  $\mathbf{R}^t, \mathbf{R}^b, \mathbf{T}^{tb}, \mathbf{T}^{bt}$  describing the response of a layer to incident

illumination. An important consequence of our transition to a frequency representation in azimuth is that each layer now in fact has a *sequence* of these matrices labeled  $\mathbf{R}_l^t, \mathbf{R}_l^b, \mathbf{T}_l^{tb}, \mathbf{T}_l^{bt}$  ( $l = 0, \dots, m$ ), which describe its response to illumination with different azimuthal Fourier modes. In this section, we show how to find these scattering matrices, starting with the simpler case of interaction with a boundary.

### 3.4.1 Scattering matrices of layer boundaries

For layer boundaries, it is straightforward to extract the scattering matrices directly from the Fourier-projected BSDF  $\mathbf{F}_l$  based on Equation (15). For this, let us partition the matrix  $\mathbf{F}_l$  into the four sub-blocks  $\mathbf{F}_l^t, \mathbf{F}_l^b, \mathbf{F}_l^{tb}$  and  $\mathbf{F}_l^{bt}$  corresponding to the different modes of reflection and transmission at the top and bottom surfaces. Then we have

$$\left[ \begin{array}{c|c} \mathbf{T}_l^{tb} & \mathbf{R}_l^b \\ \hline \mathbf{R}_l^t & \mathbf{T}_l^{bt} \end{array} \right] = \pi(1 + \delta_{0l}) \left[ \begin{array}{c|c} \mathbf{F}_l^{tb} & \mathbf{F}_l^b \\ \hline \mathbf{F}_l^t & \mathbf{F}_l^{bt} \end{array} \right] \mathbf{W} \bar{\mathbf{M}}. \quad (16)$$

In Section 5 we look at specific scattering models to find  $\mathbf{F}_l$ .

Note that this matrix layout is related to the ordering and interpretation of the discrete elevation angle cosines  $\mu_i$ . In our implementation, they are arranged in increasing order from  $-1$  to  $+1$ , where a positive value indicates illumination traveling downwards into the direction of increasing optical depth  $\tau$ .

### 3.4.2 The discrete ordinates method

Several different techniques exist that can be used to solve for the scattering matrices of medium layers. In our system, we implemented the *discrete ordinates method* and *adding-doubling* techniques; we review both here for completeness. Rearranging the terms of the projected and discretized version of the radiative transfer equation (14) yields

$$\begin{aligned} \mathbf{M} \frac{d\Phi_l(\tau)}{d\tau} &= -\Phi_l(\tau) + \pi(1 + \delta_{0l}) \mathbf{P}_l \mathbf{W} \Phi_l(\tau) \\ \Leftrightarrow \frac{d\Phi_l(\tau)}{d\tau} &= \underbrace{\mathbf{M}^{-1} (-\mathbf{I} + \pi(1 + \delta_{0l}) \mathbf{P}_l \mathbf{W})}_{=: \mathbf{A}_l} \Phi_l(\tau) \\ \Leftrightarrow \frac{d\Phi_l(\tau)}{d\tau} &= \mathbf{A}_l \Phi_l(\tau) \end{aligned}$$

This is a system of first-order ordinary differential equations, which can be solved with standard numerical techniques. Using a non-symmetric eigenvalue decomposition  $\mathbf{A}_l = \mathbf{V} \Lambda \mathbf{V}^{-1}$ , its solutions take on the form

$$\Phi_l(\tau) = \mathbf{V} e^{\Lambda \tau} \mathbf{c}$$

where  $\mathbf{c}$  captures the boundary conditions. The  $\mathbf{R}$  and  $\mathbf{T}$  matrices are then found by solving for  $\mathbf{c}$  corresponding to a unit amount of radiance arriving from the different elevation angle cosines  $\mu_1, \dots, \mu_n$ , and then evaluating  $\Phi_l(t)$  and  $\Phi_l(b)$  to find the scattered illumination at the top and bottom. This can all be accomplished in one big matrix operation:

$$\left[ \begin{array}{c|c} \mathbf{T}_l^{tb} & \mathbf{R}_l^b \\ \hline \mathbf{R}_l^t & \mathbf{T}_l^{bt} \end{array} \right] = \left[ \begin{array}{c} \mathbf{V}^\downarrow e^{\Lambda b} \\ \mathbf{V}^\uparrow e^{\Lambda t} \end{array} \right] \left[ \begin{array}{c} \mathbf{V}^\downarrow e^{\Lambda t} \\ \mathbf{V}^\uparrow e^{\Lambda b} \end{array} \right]^{-1} \quad (17)$$

where  $\mathbf{V}^\downarrow$  and  $\mathbf{V}^\uparrow$  are the  $n/2 \times n$  sub-blocks of  $\mathbf{V}$  corresponding to the upwards and downwards radiance. A total of  $m$  separate  $n \times n$  eigendecompositions and matrix inversions must be performed.

A downside of the discrete ordinates method is that the linear system in (17) can be badly conditioned when dealing with layers that have a very large optical depth. Stamnes and Conklin [1984] propose several workarounds, but these involve additional complications. In our experiments, we ran into occasional numerical robustness issues with this method and thus generally prefer the adding-doubling approach. One exception are layers with parameters continuously varying in depth, described in the following section, which are easier to handle with the semi-analytic approach of discrete ordinates.

**Heterogeneity:** By a straightforward extension of the discrete ordinates method, it is possible to handle layers that are heterogeneous in depth. For instance, suppose that

$$\frac{d\Phi_l(\tau)}{d\tau} = \mathbf{A}_l(\tau) \Phi_l(\tau)$$

where  $\mathbf{A}_l(\tau) : \mathbb{R} \rightarrow \mathbb{R}^{n \times n}$  is polynomial in  $\tau$  and specifies the medium properties as a function of depth. Then

$$\Phi_l(\tau) = e^{\int \mathbf{A}_l(\tau) d\tau} \mathbf{c}$$

where the exponent now contains the antiderivative of  $\mathbf{A}_l(\tau)$ . Evaluation of this matrix exponential is more costly, since we cannot simply precompute  $\mathbf{V}$  and  $\Lambda$ . We must thus perform the eigenvalue decomposition twice, once for  $\tau = t$  and once for  $\tau = b$ . For the simple case of a layer whose properties interpolate linearly between reference values  $\mathbf{A}^t$  at the top and  $\mathbf{A}^b$  at the bottom, we have

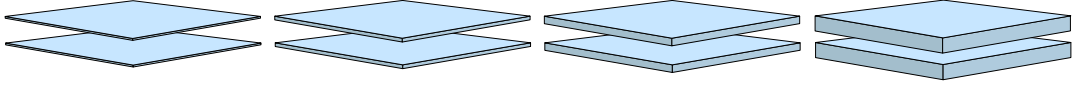
$$\mathbf{A}_l(\tau) = \frac{1}{b-t} \left( \mathbf{A}_l^t(b-\tau) + \mathbf{A}_l^b(\tau-t) \right)$$

and

$$\int \mathbf{A}_l(\tau) d\tau = \frac{\tau}{2(b-t)} \left( \mathbf{A}_l^t(2b-\tau) + \mathbf{A}_l^b(\tau-2t) \right) + C$$

### 3.4.3 The adding-doubling method

Several different techniques exist that can be used to solve for the scattering matrices of medium layers. In our system, we implemented the *discrete ordinates method* and *adding-doubling* techniques, and found the adding-doubling method to be generally preferable due to its robustness. Adding-doubling builds on the property that, as a function of optical depth, multiple scattering is a higher-order effect. For sufficiently thin layers, the portion of multiply scattered illumination is so minuscule that it can be neglected entirely. On the other hand, scattering matrices of layers with *at most* a single scattering event are easily obtained, since they admit an analytic solution. The idea of adding-doubling then is as follows: after computing the scattering matrices of a very thin layer (thin enough that multiple scattering can be neglected), the results of Section 3 are used to find the scattering matrices of a layer twice the thickness, by joining two identical layers. The layer is repeatedly doubled until it has the desired thickness.



Since  $\tau$  increases exponentially, even very thick layers can be processed rapidly.

In our implementation, we start with a depth of  $d\tau = 2^{-15}$ . To obtain layers with thicknesses other than powers of two times  $d\tau$ , we first represent the number  $\lfloor (b - t)/d\tau \rfloor$  in base 2 (where  $b - t$  is the desired thickness). A simple loop then iterates through the digits in increasing magnitude and adds a layer of thickness  $2^i d\tau$  on top of the partially generated layer whenever the  $i$ -th bit is 1.

Returning again to the projected and discretized radiative transfer equation (14), note that it describes how one “unit” of optical depth of the ambient medium locally influences the radiance function:

$$\frac{d\Phi_l(\tau)}{d\tau} = \mathbf{M}^{-1} (-\mathbf{I} + \pi(1 + \delta_{0l})\mathbf{P}_l\mathbf{W}) \Phi_l(\tau).$$

To obtain the scattering matrices of a thin layer with optical depth  $d\tau$ , we can then simply use the above differential equation as the linear term of a Taylor expansion. With some liberty in notation, this can be interpreted as

$$\Phi_l^{\text{after}} = \Phi_l^{\text{before}} + d\tau \left[ \mathbf{M}^{-1} (-\mathbf{I} + \pi(1 + \delta_{0l})\mathbf{P}_l\mathbf{W}) \right] \Phi_l^{\text{before}}$$

More formally, let us partition the matrix  $\mathbf{P}_l$  into the four sub-blocks  $\mathbf{P}^t, \mathbf{P}^b, \mathbf{P}^{tb}$  and  $\mathbf{P}^{bt}$  corresponding to the different modes of reflection and transmission at the top and bottom surfaces. Then we have

$$\left[ \begin{array}{c|c} \mathbf{T}_l^{tb} & \mathbf{R}_l^b \\ \hline \mathbf{R}_l^t & \mathbf{T}_l^{bt} \end{array} \right] = \mathbf{I} + d\tau \mathbf{M}^{-1} \left( -\mathbf{I} + \pi(1 + \delta_{0l}) \left[ \begin{array}{c|c} \mathbf{P}_l^{tb} & \mathbf{P}_l^b \\ \hline \mathbf{P}_l^t & \mathbf{P}_l^{bt} \end{array} \right] \mathbf{W} \right)$$

---

**Algorithm 1** Solve for the scattering matrices of a layered material

---

```
1 function SOLVE-SCATTERING-MATRICES(structure,  $n$ ,  $m$ )  
2   for  $l \leftarrow 0$  to  $m$  do ▷ For each Fourier mode  
3      $\hat{\mathbf{R}}_l^t, \hat{\mathbf{R}}_l^b \leftarrow \mathbf{0}, \hat{\mathbf{T}}_l^{tb}, \hat{\mathbf{T}}_l^{bt} \leftarrow \mathbf{I}$  ▷ Initialize as clear layer  
4     for  $L$  in structure do ▷ Iterate over structure  
5       if  $L$  is a boundary layer then  
6         Compute  $\mathbf{F}_l$  ▷ Section 5.2  
7         Extract  $\mathbf{R}_l^t, \mathbf{R}_l^b, \mathbf{T}_l^{tb}, \mathbf{T}_l^{bt}$  ▷ Section 3.4.1  
8       else if  $L$  is a medium layer then  
9         Compute  $\mathbf{P}_l$  ▷ Section 5.1  
10        Solve for  $\mathbf{R}_l^t, \mathbf{R}_l^b, \mathbf{T}_l^{tb}, \mathbf{T}_l^{bt}$  ▷ Section 3.4  
11        Use the adding equations to merge  $\mathbf{R}_l^t, \mathbf{R}_l^b, \mathbf{T}_l^{tb}, \mathbf{T}_l^{bt}$  into  $\hat{\mathbf{R}}_l^t, \hat{\mathbf{R}}_l^b, \hat{\mathbf{T}}_l^{tb}, \hat{\mathbf{T}}_l^{bt}$  ▷ Section 3.1  
12 return  $\hat{\mathbf{R}}_l^t, \hat{\mathbf{R}}_l^b, \hat{\mathbf{T}}_l^{tb}, \hat{\mathbf{T}}_l^{bt}$  ( $l = 0, \dots, m$ )
```

---

which tells us how to find the scattering matrix of the initial layer of depth  $d\tau$ , which is required to start up the adding and doubling process discussed above, from the phase function matrices  $\mathbf{P}$ .

So far, we have explained the basic mathematical framework of our system, which consists of a directional basis and the requisite methods to turn the matrix representations of phase functions and BSDFs in that basis into a scattering matrix for any layered material. The remainder of the paper is structured as follows: Section 4 gives an overview of the core algorithm and ties together later sections. Section 5 shows how to find the matrix representations  $\mathbf{P}_l$  and  $\mathbf{F}_l$  of relevant phase functions and BSDF models that we required in Sections 3.4.1-3.4.3. Section 5.4 fixes an energy loss problem in traditional microfacet models that causes difficulties in layered BRDFs, and Section 6 explains how to efficiently evaluate and importance sample our model in a renderer. Finally, Section 7 demonstrates applications of our model and Section 8 concludes the paper.

## 4 Algorithm overview

Algorithm 1 implements the central component that computes the Fourier modes of the reflection and transmission matrices for each layer, which are subsequently combined using the adding equations. Inputs to this algorithm are a structural model of the material consisting of the phase functions and optical depth of layers, the BSDFs of boundaries, as well as the targeted discretization  $n$  in  $\mu$  and  $\mu'$  and the number of Fourier expansion coefficients  $m$  for the azimuth difference angle  $\phi - \phi'$ . The discretization is related to the accuracy of the model, and in Section 5.7 we present conservative bounds on these parameters.

This entire computation is an offline process in the sense that it is executed before rendering starts. The output of this process is a set of  $n \times n$  matrices  $\mathbf{R}_l^t, \mathbf{R}_l^b, \mathbf{T}_l^{tb}, \mathbf{T}_l^{bt}$  ( $l = 0, \dots, m$ ) that characterize the material's response to illumination. To use this repre-

sensation in modern rendering systems, we augment it with auxiliary tables used for importance sampling, which is covered in Section 6.

Note that the high level structure of Algorithm 1 itself is not new, being a combination of standard techniques in 1D linear transport theory. The key contributions of this paper follow in the subsequent sections and focus on making each of the steps sufficiently general and scalable to tackle relevant problems in rendering.

**Sparsity:** At this point, we make an observation with important implications regarding the scalability of our approach:

1. To represent very peaked reflectance functions, we require many Fourier coefficients, but this is only the case for a small set of elevation pairs  $(\mu, \mu')$ . For instance, in the case of specular reflection, the expansions have high frequencies only when  $\mu \approx \mu'$  and low frequencies or even zeroes elsewhere.
2. Smoother reflectance functions are nonzero over many pairs  $(\mu, \mu')$ , but they are low frequency in the azimuth difference angle  $\phi - \phi'$ , and thus their Fourier series decay rapidly.

Scattering matrices of high frequency materials expressed in Chandrasekhar’s [1960] directional basis are *sparse*; our system therefore relies on sparse linear algebra techniques, allowing us to go to very high orders to represent even mirror-like materials without ringing or other artifacts (Figure 2), while generating BSDF representations that require comparably little storage. We have not found any references of this property in the literature and believe that we are the first to exploit it.

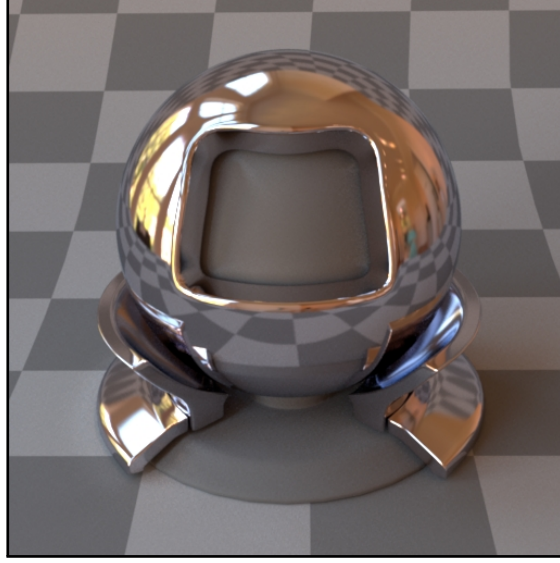
We now turn to the computation of  $\mathbf{P}_l$  and  $\mathbf{F}_l$  on lines 6 and 9.

## 5 Scattering models

Our system supports several kinds of scattering functions: for layer boundaries of dielectrics and conductors, we use the microfacet model proposed by Walter et al. [2007], and medium layers are modeled using linear combinations of the Henyey-Greenstein [1941] phase function and the von Mises-Fisher lobe proposed by Gkioulekas et al. [2013]. The main difficulty in deriving the matrices  $\mathbf{P}_l$  and  $\mathbf{F}_l$  lies in finding Fourier expansions

$$p_l(\mu, \mu') = \mathcal{F}_l [p(\mu, \mu', \cdot)] = \frac{2 - \delta_{0l}}{\pi} \int_0^\pi p(\mu, \mu', \phi) \cos(l\phi) d\phi,$$

for phase functions  $p$  and analogous for BSDFs  $f$ . The dependence on the elevations  $\mu$  and  $\mu'$  is simple as it is handled by discretization. We begin by looking at expansions of the phase function.



**Figure 2:** Frequency-based representations are usually impractical when trying to represent specular materials like this chrome object with Beckmann roughness  $\alpha = 0.01$ . We projected this material into a basis with  $m = 9763$  Fourier series terms and  $n = 503$  discretizations in  $\mu_i$  and  $\mu_o$ , which would normally produce about 28 GiB of dense coefficient data. By exploiting sparsity and our efficient Fourier projections, we require only 51.3 MiB of coefficients (0.19%) computed in 9.6 seconds; rendering took 1.4 minutes.

## 5.1 Phase functions

### 5.1.1 Henyey-Greenstein phase function

The Henyey-Greenstein (HG) phase function is a widely used one-dimensional family of phase functions with a single parameter  $g \in [-1, 1]$ , which specifies the medium's disposition of scattering light into the backward or forward direction. As a function of  $\gamma$ , the angle between the incident and outgoing directions, it is defined as

$$p(\cos \gamma) = \frac{1 - g^2}{4\pi (1 + g^2 - 2g \cos \gamma)^{3/2}}. \quad (18)$$

To find  $p_l$ , Stam [2001] used the following series, which relies on identities of associated Legendre functions:

$$p_l(\mu, \mu') = (2 - \delta_{0l}) \sum_{k=l}^{\infty} (2k+1) g^k \frac{(k-l)!}{(k+l)!} P_k^l(\mu) P_k^l(\mu') \quad (19)$$

We found this series to converge very slowly, particularly for high  $g$ . Instead, we use a technique by Yanovitskij [1997b] to rapidly and accurately compute the coefficients in



one pass using recurrences. For completeness, a C++ implementation of this method is given in Listing 1.

We wish to highlight a curious aspect of Yanovitskij's recurrence because it will resurface in the next section. His derivation shows that any three successive Fourier coefficients of the HG model relate as

$$(2l + 1)p_{l+2} = (l + 1)\rho p_{l+1} - (2l + 3)p_l, \quad (20)$$

where  $\rho \in \mathbb{R}$  does not depend on  $l$ . This suggests the following simple implementation: after computing  $p_0$  and  $p_1$  using an arbitrary numerical or analytic approach, simply perform one sweep for  $l = 2, \dots, m$ , each time using Equation (20) to find the next  $p_l$  from  $p_{l-1}$  and  $p_{l-2}$ . However, this does not work: after a few iterations, severe cancellation and error amplification in Equation (20) lead to errors that are larger than the magnitude of the correct answer. Yanovitskij therefore uses the recurrence *the other way*, going from  $p_{l+2}$  and  $p_{l+1}$  to  $p_l$ , where it is numerically well-behaved. This leads to the somewhat unusual situation of having to start a recurrence at the *end* of a desired range rather than its beginning, but the resulting implementation is fast and numerically stable.

### 5.1.2 von Mises–Fisher phase function

Due to its inherent simplicity, the HG model is a common default choice when simulating anisotropic volumetric scattering, but in a recent study, Gkioulekas et al. [2013] analyzed the perceptual significance of different phase function spaces and recommended switching to a larger space containing linear combinations of the HG model and lobes of the von Mises–Fisher distribution defined as

$$p_{\text{vMF}}(\gamma) = \frac{\kappa}{4\pi \sinh \kappa} e^{\kappa \cos \gamma} \quad (21)$$

We derive a recurrence for this phase function model which turns out to be useful a second time to compute Fourier expansions of rough boundaries in Section 5.2. We begin by noting that  $\cos \gamma$  expressed in terms of  $\mu, \phi$  and  $\mu', \phi'$  is equal to

$$\cos \gamma = \mu\mu' + \sqrt{(1 - \mu^2)(1 - \mu'^2)} \cos(\phi - \phi'). \quad (22)$$

After rewriting Equation (21) in terms of the azimuthal difference angle  $\phi_d = \phi - \phi'$  via (22) and applying an identity of the hyperbolic sine we have

$$p_{\text{vMF}}(\phi_d) = \frac{\kappa}{2\pi(1 - e^{-2\kappa})} e^{A+B \cos \phi_d} \quad (23)$$

where  $A = \kappa(\mu\mu' - 1)$  and  $B = \kappa\sqrt{(1 - \mu^2)(1 - \mu'^2)}$  do not depend on  $\phi_d$  and can thus be considered constants for the purpose of this derivation.

```

void hg_fseries(double mu_o, double mu_i, double g, int k, std::vector<double> &coeff){
    /* Compute A and B coefficients */
    double a = 1 + g*g - 2*g*mu_i*mu_o;
    double b = -2 * g * sqrt((1-mu_i*mu_i) * (1-mu_o*mu_o));

    /* Find the first two Fourier coefficients using elliptic integrals */
    double absB = fabs(b), arg = sqrt(2*absB / (a+absB));
    double K = boost::math::ellint_1(arg), E = boost::math::ellint_2(arg);
    double sqrtAB = sqrt(a+absB), temp = (1-g*g) * 0.5 / (M_PI * M_PI);
    double coeff0 = (E * temp * sqrtAB) / (a*a - b*b);
    double coeff1 = b == 0 ? 0 :
        (signum(b) * temp / (absB * sqrtAB) * (K - a / (a-absB) * E));

    int m = std::max(k, 500); /* Allocate temporary memory for ratios */
    double *s = (double *) alloca(sizeof(double) * (m + 1));

    /* Compute the ratio of the m and m+1-th term using a 2nd-order Taylor expansion */
    double z = a / sqrt(a*a - b*b), delta = z / sqrt(z*z-1);
    s[m] = (1 + 1 / (double) (2*m) - (1+3*z) / (double) (8*m*m)) * sqrt((z-1) / (z+1));

    do { /* Work backwards using a recurrence */
        --m;
        s[m] = (2*m+3) / (4*(m+1) * delta - (2*m+1) * s[m+1]);
    } while (m != 0);

    double C = 0.0;
    if (s[0] != 0)
        C = coeff1 / (coeff0 * s[0]);

    /* Multiply all ratios together to get the desired coefficients */
    coeff.push_back(coeff0);

    double prod = coeff0 * C * 2;
    for (int j=0; j<k-1; ++j) {
        prod *= s[j];
        if (j % 2 == 0)
            coeff.push_back(prod);
        else
            coeff.push_back(prod * signum(g));
    }
}

```

**Listing 1:** A C++ implementation for computing  $P_l$  matrices of the Henyey-Greenstein model (based on the recurrence by Yanovitskij). This code uses the Boost library to evaluate the elliptic integral expressions.

Using the Jacobi-Anger expansion (Abramowitz and Stegun, 9.6.34), we turn the trigonometric exponential in (23) into a Fourier series involving modified Bessel functions of the first kind:

$$e^{A+B \cos \theta} = e^A \left[ I_0(B) + 2 \sum_{l=1}^{\infty} I_l(B) \cos(l\theta) \right] \quad (24)$$

where

$$I_l(z) = \left(\frac{z}{2}\right)^l \sum_{i=0}^{\infty} \frac{\left(\frac{1}{4}z^2\right)^i}{i! \Gamma(l+i+1)}.$$

Technically, this completes the derivation of the Fourier projection, but in practice Bessel functions are very costly to evaluate, and in our system, they can be invoked with arguments that lead to overflows in floating point arithmetic due to their fast growth (consider that  $I_0(1000) \approx 2.5 \cdot 10^{432}$ ); this is particularly an issue with uses of this expansion later in the paper. To address these issues, we start by noting that Equation (24) actually takes on very reasonable values in the interval  $[0, 1]$  since  $A + B \cos \phi_d \leq 0$ . To always remain in the representable number range, it is thus key that we incorporate the exponential scaling by  $e^A$  into the computation of the coefficients. We use the following expression for computing the  $l$ -th scaled Bessel function:

$$e^A I_l(B) = \underbrace{e^{-B} I_0(B)}_{= I_0^e(B)} e^{A+B} \prod_{j=1}^l \frac{I_j(B)}{I_{j-1}(B)} \quad (25)$$

There are several things to note about this expression: the first term  $I_0^e(B)$  is the exponentially scaled modified Bessel function of order zero; we evaluate it using the `I0E` function provided in Cephes mathematical library. The second term accounts for the fact that we needed to scale by  $e^A$  instead of  $e^B$ . The last term is a product of *ratios* of Bessel functions, which are close to 1 and easily representable. These ratios satisfy a recurrence relation which we use not only to evaluate (25) but also to efficiently find all series terms of (21) for a pair of angles  $\mu, \mu'$  (i.e. for constant  $A$  and  $B$ ) in one sweep. The recurrence is given by

$$\frac{I_{l+1}(B)}{I_l(B)} = \frac{I_{l-1}(B)}{I_l(B)} - \frac{2l}{B}. \quad (26)$$

Interestingly, similar to the Henyey-Greenstein recurrence in Section 5.1.1 this relation also suffers from catastrophic cancellation and error magnification when used in the upward sense (i.e. computing the ratio for  $l+1$  from the previous one at  $l$ ), while being stable when used in the *downward* sense:

$$\frac{I_l(B)}{I_{l-1}(B)} = \frac{B}{2l + B \frac{I_{l+1}(B)}{I_l(B)}} \quad (27)$$

```

double mbessel_ratio(Float k, double B) {
    const double eps = std::numeric_limits<double>::epsilon(),
        invTwoB = 2.0 / B;

    double i = (double) k,
        D = 1.0 / (invTwoB * i++),
        Cd = D, C = Cd;

    while (fabs(Cd) > eps * fabs(C)) {
        double coeff = invTwoB * i++;
        D = 1 / (D + coeff);
        Cd *= coeff * D - 1;
        C += Cd;
    }

    return C;
}

```

**Listing 2:** A C++ implementation that evaluates the continued fraction in Equation (28) via Steed’s method.

Our implementation then starts with the maximum expansion order  $l = m$ , and computes the ratios  $I_l/I_{l-1}$ ,  $I_{l-1}/I_{l-2}$  down to  $I_1/I_0$  using recurrences. However, this requires knowing the *last* ratio  $I_l/I_{l-1}$  to bootstrap the recurrence formula: for this purpose, we use a quickly converging continued fraction representation based on Gauss’ work on ratios of hypergeometric functions (see Gautschi and Slavik [1978] for a general discussion):

$$\frac{I_l(B)}{I_{l-1}(B)} = \frac{1}{\frac{\frac{2}{B}l + \frac{1}{\frac{2}{B}(l+1) + \frac{1}{\frac{2}{B}(l+2) + \dots}}}} \quad (l > 0) \quad (28)$$

We evaluate this continued fraction using Steed’s method, which yields a very accurate routine shown in Listing 2. Combining the continued fraction representation, the recurrence over ratios and the exponentially scaled function  $I_0^e$ , we obtain an efficient and stable method for computing azimuthal Fourier series of the von Mises–Fisher distribution. An implementation of this routine is shown in Listing 3.

## 5.2 Boundaries between layers

To model boundaries of dielectrics and conductors, we use the microfacet model proposed by Walter et al. [2007]. Microfacet models describe the interaction of light with random surfaces composed of microscopic dielectric or conducting facets that are oriented according to a microfacet distribution. Integration over this distribution then leads to simple analytic expressions that describe the expected reflection and transmission properties at a macroscopic scale. Validations against real-world measure-

```

void expcos_fseries(double A, double B, int m, std::vector<double> &coeffs) {
    coeffs.resize(m+1);

    /* Determine the last ratio and work downwards */
    coeffs[m] = mbessel_ratio(B, m);
    for (int i=m-1; i>0; --i)
        coeffs[i] = B / (2*i + B*coeffs[i+1]);

    /* Evaluate the exponentially scaled I0 and correct scaling */
    coeffs[0] = std::exp(A+B) * cephes::i0e(B);

    /* Apply the ratios & factor of two upwards */
    double prod = 2*coeffs[0];
    for (int i=1; i<m+1; ++i) {
        prod *= coeffs[i];
        coeffs[i] = prod;
    }
}

```

**Listing 3:** A C++ implementation that computes series coefficients of the Jacobi-Anger expansion in Equation (24).

ments have shown that microfacet models compare favorably against other families of parametric BRDF models [Ngan et al. 2005].

We begin with a short review of the microfacet model by Walter et al., specifically the variant that uses the Beckmann distribution derived from Gaussian random surfaces. This model consists of a reflection and a transmission term

$$f(\mu_i, \phi_i, \mu_o, \phi_o) = f_r(\mu_i, \mu_o, \phi_i - \phi_o) + f_t(\mu_i, \mu_o, \phi_i - \phi_o). \quad (29)$$

The reflection term  $f_r$  is defined as

$$f_r(\mu_i, \mu_o, \phi_d) = \frac{F(\mu_h)D(\mu_h)G(\mu_i, \mu_o)}{4|\mu_i\mu_o|}$$

where  $F$  specifies the Fresnel reflectance,  $D$  is the Beckmann distribution,  $G$  is a shadowing-masking term, and  $\mu_h$  denotes the cosine of the angle between the normal and the half-direction vector of the incident and outgoing directions. The refractive case is defined analogously but involves a modified half direction vector and different weighting terms. Note that while the paper by Walter et al. only concerns itself with dielectrics, it is straightforward to generalize the model to also handle conductors by replacing  $F$  with the general unpolarized Fresnel reflectance term for boundaries with a complex-valued relative index of refraction and setting  $f_t = 0$ . We refer to the original papers for many further details and a full discussion of the the refraction term  $f_t$ .

To compute the azimuthal modes of  $f$  we must again integrate

$$\mathcal{F}_l[f(\mu, \mu', \cdot)] = \frac{2 - \delta_{0l}}{\pi} \int_0^\pi f(\mu, \mu', \phi_d) \cos(l\phi_d) d\phi_d. \quad (30)$$

However, we were not able to find an analytic expression for this integral due to the significant complexity of the integrand. Forced to turn to numerical integration, we encountered further problems:

- $f$  varies greatly in magnitude with respect to  $\phi_d$ : usually, only a tiny portion of the of the domain contributes to the integral.
- Higher-order Fourier basis functions are oscillatory, i.e. they have a large number of lobes of opposing signs, which almost (but not quite) cancel each other.

The combination of these properties makes both general-purpose and special oscillatory integration methods impracticably slow. To sidestep these difficulties, we propose a semi-analytic integration routine tailored to this specific problem.

We note that, although the full expression of the BSDF  $f$  has several parts that depend on  $\phi_d$ , the exponential term in the Beckmann microfacet distribution is the one that, by far, dominates its behavior. Splitting the integrand of (30) into this exponential term and a function  $f_{\text{rem}}$  containing the remaining terms produces

$$\mathcal{F}_l[f(\mu_i, \mu_o, \cdot)] = \frac{2 - \delta_{0l}}{\pi} \int_0^\pi f_{\text{rem}}(\phi_d) e^{A+B \cos \phi_d} \cos(l\phi_d) d\phi_d$$

where in the reflective case  $A$  and  $B$  are defined as

$$A = \frac{\mu_i^2 + \mu_o^2 - 2}{\alpha^2(\mu_i - \mu_o)^2}, \quad B = \frac{2\sqrt{1 - \mu_i^2}\sqrt{1 - \mu_o^2}}{\alpha^2(\mu_i - \mu_o)^2}. \quad (31)$$

In the refractive case, they are given by

$$A = \frac{\eta_i^2(\mu_i^2 - 1) + \eta_o^2(\mu_o^2 - 1)}{\alpha^2(\eta_i\mu_i - \eta_o\mu_o)^2}, \quad B = \frac{2\eta_i\eta_o\sqrt{1 - \mu_i^2}\sqrt{1 - \mu_o^2}}{\alpha^2(\eta_i\mu_i - \eta_o\mu_o)^2}. \quad (32)$$

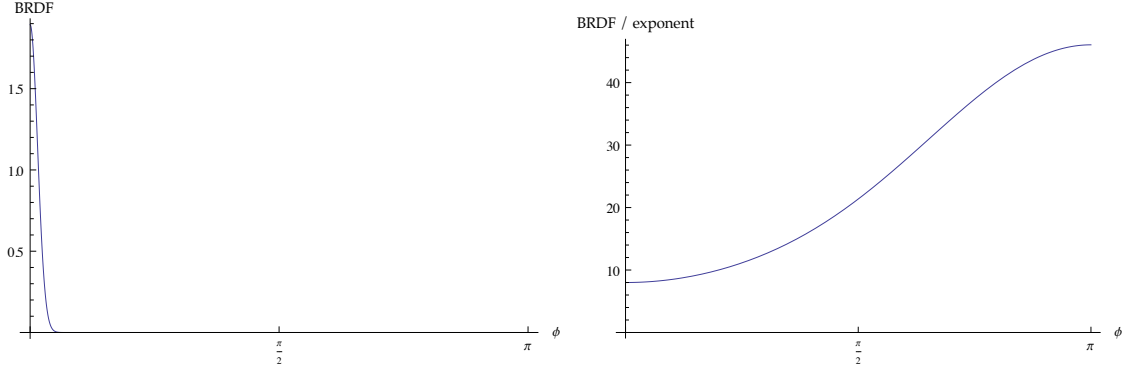
We observe a striking similarity to the exponential-of-cosine Fourier series in Equation (24) encountered during our treatment of the von Mises–Fisher phase function, with the main change being the extra term  $f_{\text{rem}}(\phi_d)$  which contains normalization and shadowing-masking terms as well as the Fresnel coefficient. Suppose for a moment that we were able to obtain series representations of these pieces *separately*, i.e. coefficients  $a_l$  and  $b_l$  such that

$$e^{A+B \cos \phi_d} = \sum_{l=0}^{\infty} a_l \cos(l\phi_d)$$

$$f_{\text{rem}}(\phi_d) = \sum_{l=0}^{\infty} b_l \cos(l\phi_d)$$

The Fourier series we actually wanted to obtain is the pointwise multiplication of these two series.

$$C(\phi_d) = e^{A+B \cos \phi_d} f_{\text{rem}}(\phi_d) = \sum_{l=0}^{\infty} c_l \cos(l\phi_d)$$



**Figure 3:** Plot of a typical configuration of the microfacet model for reflection,  $f_r$ , as a function of  $\phi_d$  ( $\mu = -0.6, \mu' = 0.5, \alpha = 0.05, \eta = 1.5$ ). **Left:** the full model, i.e.  $C(\phi_d)$ , **Right:** The same function, but with the exponential term removed, varies smoothly and is well-approximated using a truncated Fourier series with only 6 terms (relative error  $< 10^{-6}$ )

At this point, we note that as a consequence of the convolution theorem, the frequency space analog to a pointwise multiplication in the  $\phi_d$  argument is the *discrete convolution* of the number sequences  $(a_n)$  and  $(b_n)$ . In particular, the coefficients  $c_i$  we seek are given by a discrete circular convolution, which takes on the form (using the convention that  $a_{-i} = a_i$ ):

$$c_i = \frac{1}{2(1 + \delta_{0i})} \left[ \delta_{0i} a_0 b_0 + \sum_{j=0}^{\infty} b_j (a_{i+j} + a_{i-j}) \right] \quad (33)$$

If  $a_l$  and  $b_l$  are easily obtained, and if one of them decays quickly enough, this yields an attractive way of finding the coefficients of the product. We found that this is indeed the case: for conductors,  $f_{\text{rem}}$  is generally smooth enough to be representable with relative error of  $10^{-6}$  using only six series terms (we conservatively use 12). For dielectrics, more coefficients are needed in certain cases, but the average is still very low, around 14-20 depending on the parameters. Importantly, changing the roughness  $\alpha$  does not change the frequency content of  $f_{\text{rem}}$ , and we can therefore depend on the robustness of our exponential-of-cosine expansion to handle low-roughness cases.

Figure 3 demonstrates the low frequency content of  $f_{\text{rem}}(\phi)$ . For the given parameters, this function can be approximated to a relative error of  $10^{-6}$  using only six Fourier coefficients. This low-frequency property holds throughout most of the parameter space (we will focus on exceptions shortly).

Our approach then is to compute *two* Fourier series and find their discrete convolution: one of the high frequency exponential, where we simply use the algorithm already developed in Section 5.1.2, and another of  $f_{\text{rem}}(\phi_d)$ , which is handled using a traditional numerical method for Fourier integrals (we use Filon quadrature [1928]).

Listing 4 implements the discussed discrete circular convolution operation in C++.

```

void fseries_convolve(const double *a, int ka, const double *b, int kb, double *c) {
    /* Input: a[0]..a[ka-1], b[0]..b[kb-1]. Output: c[0]..c[ka+kb-1] */
    for (int i=0; i<ka+kb-1; ++i) {
        double sum = 0.0;

        for (int j=0; j<std::min(kb, ka-i); ++j)
            sum += b[j]*a[i+j];

        for (int j=std::max(0, i-ka+1); j<std::min(kb, i+ka); ++j)
            sum += b[j]*a[abs(i-j)];

        if (i < kb)
            sum += b[i]*a[0];

        if (i == 0)
            sum = 0.5 * (sum + a[0]*b[0]);

        c[i] = 0.5 * sum;
    }
}

```

**Listing 4:** C++ implementation of a truncated version of the circular convolution in Equation (33)

The next sections will focus on computing series expansions of the exponential and the remaining terms.

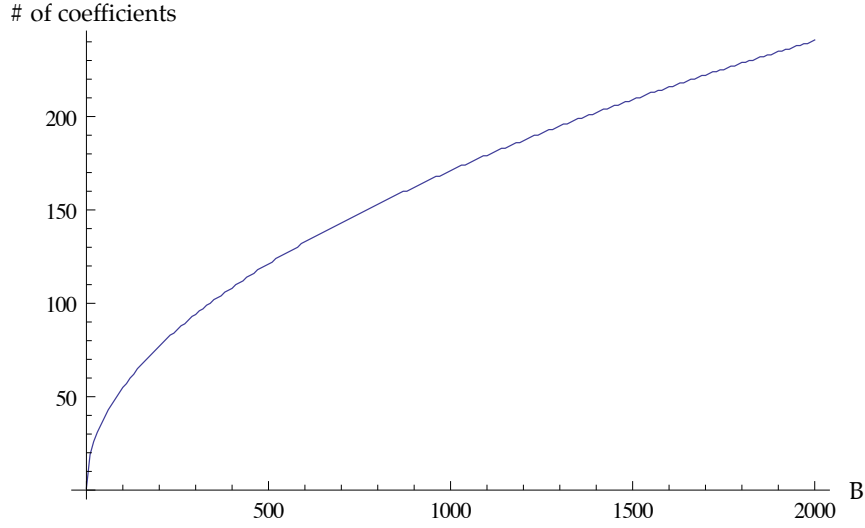
**Measured materials:** It is also possible to import measured materials into our system to compose them with other layers. We have implemented this for materials in the database of Matusik et al. [2003], for which we approximately Fourier-project the BSDF for each pair  $\mu_i, \mu_o$  by densely sampling it in azimuth  $[0, 2\pi]$  and applying a Fast Fourier Transform. This is relatively fast but only an approximation; also the required resolution depends on the material’s specularity and must be determined manually. We leave better integration schemes for such “black box” data as a future work.

### 5.3 Additional implementation considerations

The previous sections presented a scheme for computing Fourier coefficients of a microfacet model by decomposing it into two parts: a high-frequency and a low-frequency term, whose respective coefficients were found separately and then convolved. However, there are two remaining issues that we must address for this to work robustly in all situations:

**Divergence of  $A$  and  $B$ :** A closer examination of the  $A$  and  $B$  constants used in the exponential term for reflection (31) and refraction (32) reveals that they can grow arbitrarily large in magnitude. In the reflective case, they diverge e.g. when  $\mu_i$  and  $\mu_o$  simultaneously tend to zero. This is bad news for our Fourier series approach,





**Figure 4:** For a relative error threshold of  $10^{-6}$ , this plot shows the required number of series terms for increasing values of  $B$

because it means that the microfacet model contains *arbitrarily high* frequency content. We cannot possibly represent these frequencies; the series must be truncated at some point, which would then introduce an unacceptable amount of ringing for sufficiently small  $\mu_i$  and  $\mu_o$ .

This ostensibly bleak outlook is unjustified: due to the foreshortening associated with surface light transport, very little energy is actually transported at these grazing angles. This means that it is fine for our representation to become approximate in this setting which, as we will see, introduces very little error overall. We therefore apply smoothing to frequencies that are too high to be represented so that no ringing occurs after truncation.

Figure 4 shows how many series terms are needed to accurately represent the exponential term with a relative error threshold of  $10^{-6}$  for different values of  $B$ . The inverse of this function is closely approximated by

$$B_{\max}(k) \approx 0.03k^{2.026} \quad (\text{relative error} \approx 0.0011)$$

For other error thresholds, we have

$$B_{\max}(k) \approx \begin{cases} 0.0337 k^{2.03865}, & \varepsilon = 10^{-5} \\ 0.0406 k^{2.04686}, & \varepsilon = 10^{-4} \\ 0.0538 k^{2.05001}, & \varepsilon = 10^{-3} \\ 0.0818 k^{2.04982}, & \varepsilon = 10^{-2} \end{cases}$$

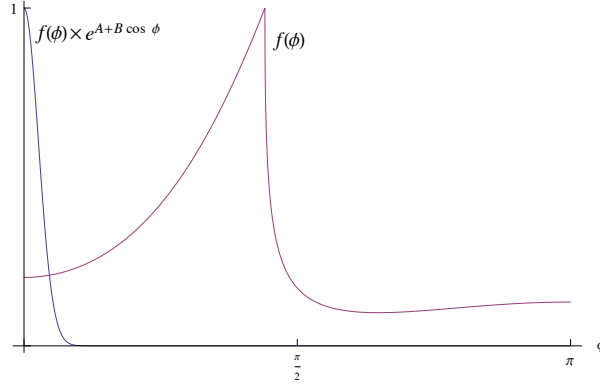
For any given number of series terms, this function tells us the maximum value of  $B$  that can be represented so that no ringing occurs after truncation (up to the chosen

error threshold). In our implementation, we compute  $A$  and  $B$  according to Equations (31) and (32) and obtain clamped  $A'$  and  $B'$  using

$$B' = \min\{B, B_{\max}(k_{\max})\}$$

$$A' = A + B - B' + \log \frac{I_0^e(B)}{I_0^e(B')}$$

where  $k_{\max}$  is the number of coefficients used in the simulation. Here,  $A'$  is chosen so that the amount of energy (i.e. the 0<sup>th</sup> order Fourier coefficient) is preserved.



**Figure 5:** When passing into a material having a smaller index of refraction, the  $f_{\text{rem}}(\phi)$  term spikes at  $\phi_{\text{crit}}$  ( $\mu_i = -0.5, \mu_o = 0.5, \eta = 1/1.5, \alpha = 0.1$ , normalized plot)

**High frequencies in  $f_{\text{rem}}(\phi)$ :** There is another part of the model that will cause difficulties unless special precautions are taken: the Fresnel reflectance and transmittance terms in  $f_{\text{rem}}(\phi)$  contain high frequencies when passing into a medium that has a smaller index of refraction (Figure 5). In particular, the function rapidly spikes (or vanishes in the refraction case) when the angle between the microfacet normal and the incident direction approaches the critical angle. In the  $(\mu_i, \mu_o, \phi)$  parameterization, this happens when  $\phi \rightarrow \phi_{\text{crit}}$ , where

$$\phi_{\text{crit}} = \cos^{-1} \frac{2\eta^2 - \mu_i\mu_o - 1}{\sqrt{1 - \mu_i^2}\sqrt{1 - \mu_o^2}} \quad (\text{reflection}), \text{ or}$$

$$\phi_{\text{crit}} = \cos^{-1} \frac{1 - \eta\mu_i\mu_o}{\eta\sqrt{1 - \mu_i^2}\sqrt{1 - \mu_o^2}} \quad (\text{refraction})$$

In most cases,  $f$  is effectively constant in the region where the exponential term takes on non-negligible values, and hence the spikes disappear due to its exponential decay.

Yet, this presents a problem for our proposed scheme for finding the Fourier transform of the combined model: if we try to fit such a function  $f_{\text{rem}}(\phi)$  using a low-order

Fourier series (e.g. with 6-12 terms) it will suffer from severe ringing *globally*, and this ringing will be present even after the discrete convolution operation.

What we'd rather like to have is a Fourier series of  $f_{\text{rem}}$  that is a very good fit on some region  $[0, \phi_{\text{max}}]$  where the exponential term takes on non-negligible values, and which is free to have arbitrary behavior elsewhere (anything it might possibly do will be dwarfed by the exponential decay). Solving for  $\phi$  in  $e^{A+B \cos \phi} / e^{A+B \cos 0} = \varepsilon$  yields

$$\phi_{\text{max}} = \cos^{-1} \frac{B + \log \varepsilon}{B}$$

Our implementation uses a configurable threshold that is set by the desired relative error goal (e.g.  $\varepsilon = 10^{-3}$ ). The next question is how such a "localized" Fourier series should be obtained. Let us define the Fourier basis functions

$$q_i(\phi) := \cos(i\phi) \quad (i = 0, 1, \dots)$$

and an inner product

$$\langle g, h \rangle = \int_0^{\phi_{\text{max}}} g(\phi) h(\phi) d\phi$$

The functions  $q_i$  clearly lose their orthogonality with respect to  $\langle \cdot, \cdot \rangle$  when  $\phi_{\text{max}} \neq \pi$ . After computing the inner products  $\langle f, q_i \rangle$ , an additional transformation is thus necessary to find the final coefficients  $a_0, \dots, a_n$ :

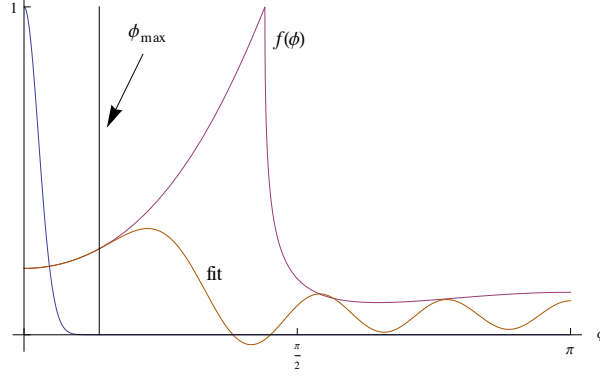
$$\begin{pmatrix} a_0 \\ \vdots \\ a_n \end{pmatrix} = \begin{pmatrix} \langle q_0, q_0 \rangle & \dots & \langle q_0, q_n \rangle \\ \vdots & & \vdots \\ \langle q_n, q_0 \rangle & \dots & \langle q_n, q_n \rangle \end{pmatrix}^{-1} \begin{pmatrix} \langle q_0, f \rangle \\ \vdots \\ \langle q_n, f \rangle \end{pmatrix}$$

The entries of this matrix can be computed analytically:

$$\langle q_i, q_j \rangle = \begin{cases} (i \cos(j\phi_{\text{max}}) \sin(i\phi_{\text{max}}) - j \cos(i\phi_{\text{max}}) \sin(j\phi_{\text{max}})) / (i^2 - j^2), & i \neq j \\ (\sin(2i\phi_{\text{max}}) + 2i\phi_{\text{max}}) / (4i), & i = j \neq 0 \\ \phi_{\text{max}}, & i = j = 0 \end{cases}$$

Note that, depending on the value of  $\phi_{\text{max}}$  and the desired number of coefficients, this fitting problem is potentially underdetermined (in the sense that several series might be a good match on the interval). We regularize the linear system by means of a singular value decomposition, where singular values close to zero ( $\sigma_i < 10^{-9}\sigma_1$ ) are associated with the null-space and consequently dropped. Figure 6 shows an example of this scheme on the previous problem case.

Finally, it may happen that  $\phi_{\text{crit}} < \phi_{\text{max}}$ , in which case some of the high frequency content "survives" the multiplication by the exponential term, and hence we must account for it. Our implementation detects this case and increases the amount of coefficients used for  $f$  from 12 (the conservative default) to 100. This case occurs very rarely in practice.



**Figure 6:** Demonstration of a Fourier series that only considers areas where the exponential term takes on non-negligible values (cf. Figure 5). With  $n = 10$  coefficients, this fit achieves a relative error of  $5 \cdot 10^{-8}$  on the interval  $[0, \phi_{\max}]$ . It does poorly elsewhere, but this is irrelevant due to the exponential decay.

## 5.4 Multiple scattering term

One issue with currently used microfacet models is that they only account for a single scattering event at the microgeometry level; light that interacts with multiple facets is effectively ignored. This means that these models incur some energy loss which grows steadily as the roughness of the interface is increased. In a simulation of layered materials with multiple rough internal boundaries, this loss is incurred many times due to interactions between layers, potentially removing significant amounts of energy.

We propose an additive correction term to the microfacet model, which reintroduces any energy lost to multiple scattering. This term is approximate—in particular, we assume that, following multiple interactions within the surface microgeometry, the scattered radiation emerges with an angular distribution that is close to diffuse. The main constraint on this correction is that it should be reciprocal like other parts of our system. The discrete analog of continuous reciprocity [Veatch 1997] in our setting is a set of matrix equations:

$$\mathbf{F}_l^t = \mathbf{F}_l^{tT}, \quad \mathbf{F}_l^b = \mathbf{F}_l^{bT}, \quad \eta_t^2 \mathbf{F}_l^{tb} = \eta_b^2 \mathbf{F}_l^{btT} \quad (l = 0, \dots, m)$$

The assumption of multiply scattered illumination emerging with an approximately diffuse profile allows us to restrict the correction to the 0<sup>th</sup> order Fourier mode (i.e.  $l = 0$ ), and to preserve reciprocity we use the following rank-1 update of  $\mathbf{F}$ :

$$\hat{\mathbf{F}}_0^t = \mathbf{F}_0^t + \mathbf{r}^t \mathbf{r}^{tT}, \quad \hat{\mathbf{F}}_0^b = \mathbf{F}_0^b + \mathbf{r}^b \mathbf{r}^{bT}, \quad \hat{\mathbf{F}}_0^{tb} = \mathbf{F}_0^{tb} + \frac{\mathbf{t}^{bt} \mathbf{t}^{tbT}}{\eta_b^2}, \quad \hat{\mathbf{F}}_0^{bt} = \mathbf{F}_0^{bt} + \frac{\mathbf{t}^{tb} \mathbf{t}^{btT}}{\eta_t^2}$$

The vectors  $\mathbf{r}^t$ ,  $\mathbf{r}^b$ ,  $\mathbf{t}^{tb}$  and  $\mathbf{t}^{bt}$  are chosen appropriately so that the final representation has no energy loss. We derived expressions for these vectors for rough conductors and

dielectrics. Our approach is related to work by Kelemen et al. [2001] who derived a continuous correction term for a specular-matte BRDF.

As a prerequisite, it will be necessary to know exactly how much energy is reflected and transmitted for a certain value of  $\mu_i$ ; in other words, we must compute the integrals of the type

$$e^t(\mu_i) = \int_0^{2\pi} \int_0^1 f(\mu_i, \mu_o, \phi_d) |\mu_o| d\mu_o d\phi_d,$$

and so on. Let  $\widehat{\mathbf{W}} := [2\pi\mu_0w_0, \dots, 2\pi\mu_nw_n] \in \mathbb{R}^{1 \times n}$ , where  $\mu_i$  and  $w_i$  are the nodes and weights of the underlying quadrature method. Then the discrete equivalents of the above integrals are given by:

$$\mathbf{e}^t = \widehat{\mathbf{W}}\mathbf{F}_0^t, \quad \mathbf{e}^b = \widehat{\mathbf{W}}\mathbf{F}_0^b, \quad \mathbf{e}^{tb} = \widehat{\mathbf{W}}\mathbf{F}_0^{tb}, \quad \mathbf{e}^{bt} = \widehat{\mathbf{W}}\mathbf{F}_0^{bt}$$

Consequently, the amount of lost energy per incident  $\mu_i$  is equal to  $\mathbf{l}^t := \mathbf{1} - \mathbf{e}^t - \mathbf{e}^{tb}$  for illumination arriving at the top and  $\mathbf{l}^b := \mathbf{1} - \mathbf{e}^b - \mathbf{e}^{bt}$  at the bottom.

To motivate the following we start by considering a simple BRDF with a single reflection lobe at the top boundary, having an energy loss of  $\mathbf{e}^t$ . In this case the correction term we require is simply a scaled version of the loss  $\mathbf{l}^t$ , i.e.

$$\mathbf{t}^t = \rho \mathbf{l}^t \tag{34}$$

and to find  $\rho$  we place the requirement that after the correction there should be no energy loss, i.e.

$$\begin{aligned} \widehat{\mathbf{W}}(\mathbf{F}_0^t + \mathbf{t}^t \mathbf{t}^{tT}) &= \mathbf{1} \\ \Leftrightarrow \mathbf{e}^t + (\rho^2 \widehat{\mathbf{W}} \mathbf{l}^t)(\mathbf{1} - \mathbf{e}^t) &= \mathbf{1} \end{aligned}$$

To satisfy this equation we set

$$\rho = 1 / \sqrt{\widehat{\mathbf{W}} \mathbf{l}^t}.$$

Our corrections for the microfacet lobes work in this way but involve some additional considerations described in the next two sections.

## 5.5 Multiple scattering term for dielectrics

In the case of dielectrics, for each  $\mu_i$  we split the correction between reflection and refraction so that the current division of energy between these lobes is preserved. This leads to the following unscaled corrections for refraction (written in component notation where  $k = 1, \dots, n$ ):

$$\widehat{\mathbf{t}}_k^{tb} = \mathbf{l}_k^t \frac{\mathbf{e}_k^{tb}}{\mathbf{e}_k^t + \mathbf{e}_k^{tb}}, \quad \widehat{\mathbf{t}}_k^{bt} = \mathbf{l}_k^b \frac{\mathbf{e}_k^{bt}}{\mathbf{e}_k^b + \mathbf{e}_k^{bt}}$$

Because of the reciprocal relationship of the two transmission lobes, we must be careful not to create too much energy on one side of the BSDF by adding a correction to the other. Hence, in this case the correction is a minimum of two terms and reads

$$\begin{aligned} \mathbf{t}_k^{tb} &= \hat{\mathbf{t}}_k^{tb} \min \left\{ \widehat{\mathbf{W}} \mathbf{t}^{bt}, \widehat{\mathbf{W}} \mathbf{t}^{tb} \frac{\eta_t^2}{\eta_b^2} \right\} \\ \mathbf{t}_k^{bt} &= \hat{\mathbf{t}}_k^{bt} \min \left\{ \widehat{\mathbf{W}} \mathbf{t}^{tb}, \widehat{\mathbf{W}} \mathbf{t}^{bt} \frac{\eta_b^2}{\eta_t^2} \right\} \end{aligned}$$

After this correction we update the energy loss vectors  $\mathbf{l}^t$  and  $\mathbf{l}^b$  and simply put the remaining lost energy onto the reflection lobes on each side of the surface using the approach of Equation (34).

## 5.6 Multiple scattering term for conductors

We consider conductors as opaque and therefore just focus on the top surface. For conductors, a simple correction would be to put all missing energy into the reflection lobe—however, this is not correct because conductors have a complex-valued index of refraction and thus naturally absorb some of the illumination, which we do not want to recover.

Our approach then is as follows: we first compute an auxiliary version of the zero-order scattering matrix  $\mathbf{F}_0^t$  that does not include the Fresnel coefficient, and compute the energy loss vector  $\mathbf{l}^t$  for this matrix instead, leading to a preliminary correction

$$\hat{\mathbf{t}}^t = \sqrt{\widehat{\mathbf{W}} \mathbf{l}^t \mathbf{l}^t}$$

To determine the correct scale factor for this correction we use a very simple model of diffuse light interreflecting inside the microfacet geometry.

After a single scattering interaction of a ray of light, the portion of the ray's energy that is eliminated due to energy loss in the BRDF is given by  $\mathbf{W} \hat{\mathbf{t}}^T / \pi$ , and thus we can think of

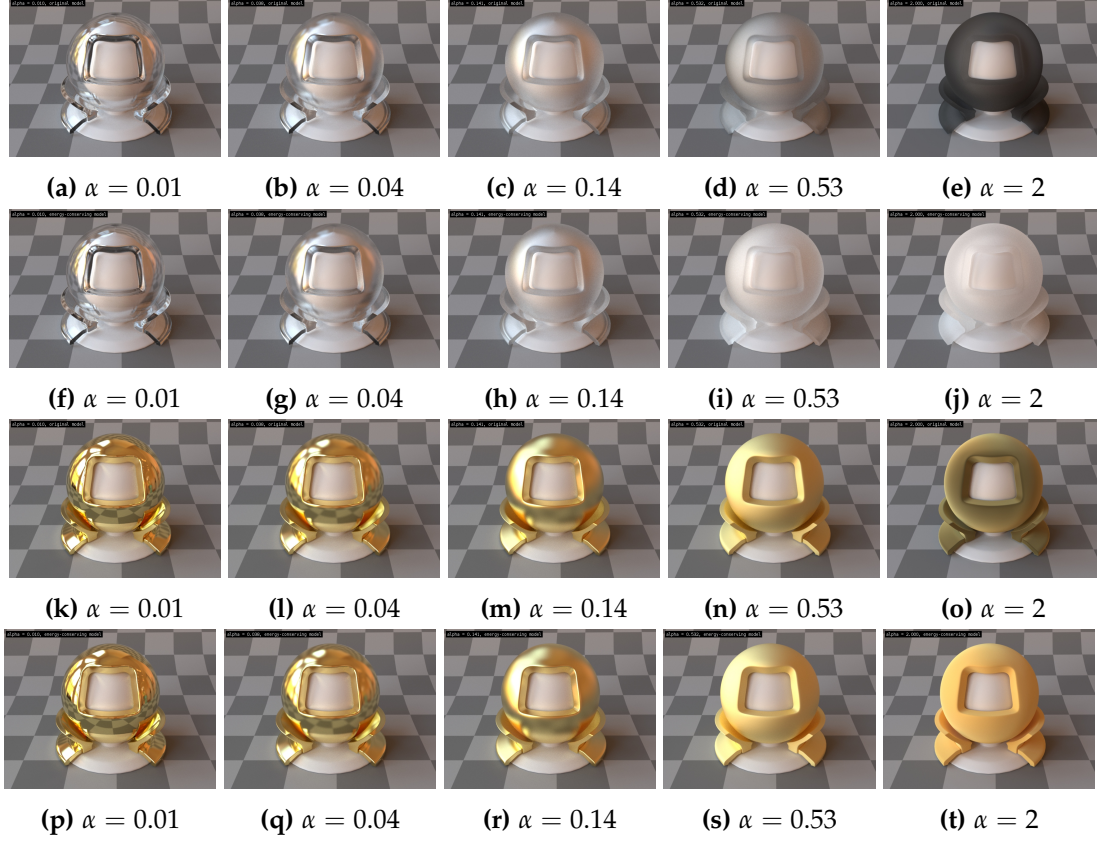
$$E = 1 - \frac{\widehat{\mathbf{W}} \hat{\mathbf{t}}^t}{\pi}$$

as the portion of light that is able to escape the surface microgeometry after a single scattering event. We assume that the portion which did not escape re-emerges as diffuse illumination that undergoes a multiple scattering process.

The next time this illumination encounters a microfacet, due to the diffuse assumption, its energy is reduced by the average Fresnel reflectance of the conductor,

$$R = 2 \int_0^1 F(\mu) \mu d\mu$$

which we compute numerically using Gaussian integration. Again, a portion  $E$  of the illumination is now able to leave the surface, and the remainder undergoes further



**Figure 7:** Traditional microfacet models for dielectrics and conductors (rows 1 and 3) suffer from energy loss that is particularly problematic in simulations of layered materials. We propose a multiple scattering term that reintroduces this energy (rows 2 and 4).

scattering events. To find  $\rho$ , we sum over all of possible paths that the lost energy could follow before exiting the surface, which turns into the following geometric series:

$$\rho = RE + R(1 - E)RE + R^2(1 - E)^2RE + \dots = \sum_{i=0}^{\infty} R^i(1 - E)^i = \frac{RE}{1 - R(1 - E)}$$

Due to this multiple scattering process, the saturation of certain conductors with very apparent coloration in the visible spectrum (e.g. copper or gold) increases when instantiated with extreme roughness values (e.g.  $\alpha = 2$ ). Figure 7 highlights the effect of our correction on dielectrics and conductors of different roughness values.

## 5.7 Error analysis

To use Algorithm 1 in practice we need a way of selecting an appropriate discretization  $n$  in elevation, and number  $m$  of Fourier expansion terms. How these parameters

should be set is not obvious; overly high values will cause unnecessary overheads while a too low value may introduce unacceptable errors. Intuitively, their choice relates to the “peakedness” of the ingredients, i.e. the parameter  $\alpha$  for boundaries, and  $g$  or  $\kappa$  for scattering layers.

We propose a heuristic for each kind of layer that specifies appropriate  $n$  and  $m$  if that layer were be represented *in isolation*. These heuristics are simple functions that map the relevant parameter to a discretization with less than 1% relative  $L^2$  representation error. We created these heuristics by bounding  $n$  and  $m$  values found via a brute force search (Figure 8).

For a material made of multiple layers  $i = 1, \dots, N$  these heuristics will generally recommend a set of incompatible parameter values  $(n_1, m_1), \dots, (n_N, m_N)$ . However, for Algorithm 1 to work we must decide on a *single* value of  $n$  and  $m$  that are used for the entire computation. For the  $n$  parameter, we simply set  $n = \max_i n_i$ . In the parameter  $m$  we do not need to be as conservative: each layer  $i$  can be thought of as a low-pass filter that removes azimuthal frequency content that is higher than order  $m_i$ . Therefore, all interior layers are “filtered” by the top and bottom layers, and hence we set  $m = \max\{m_1, m_N\}$ .

To analyze the approximation errors of our system, and to find viable heuristics for the individual layers, we define the weighted relative  $L^2$  error of the tabulation  $\tilde{f}$  with respect to an analytic BSDF model  $f$  as

$$\text{Relative } L^2 \text{ Error} = \left[ \frac{\int_{-1}^1 \int_{-1}^1 \int_0^\pi \left( |\mu_i \mu_o| (f(\mu_i, \mu_o, \phi) - \tilde{f}(\mu_i, \mu_o, \phi)) \right)^2 d\phi d\mu_i d\mu_o}{\int_{-1}^1 \int_{-1}^1 \int_0^\pi (|\mu_i \mu_o| f(\mu_i, \mu_o, \phi))^2 d\phi d\mu_i d\mu_o} \right]^{1/2} \quad (35)$$

An analogous error can be defined for phase functions without the  $\mu\mu'$  weighting term, which accounts for the reduced energy on surfaces at grazing angles due to foreshortening.

We ran a program that instantiated all supported layer types with many different parameter values, each time searching for suitable values of  $n$  and  $m$ . In particular, we tried to find the smallest  $n$  and  $m$  subject to the cost function  $c(n, m) = n^2 m$  denoting the number of parameters in the dense case, which led to less than 1% relative error in our discretized and Fourier-expanded representation.

An example of the output of this program can be seen in Figure 8. The black dots in the normal and log plots in the top row show the  $n$  and  $m$  values found by the search. For rough interfaces, we bound both  $m$  and  $n$  by functions of the type

$$\{n, m\}(\alpha) = \max \left\{ a + b\alpha \log(\alpha)^4, c + d\alpha^{-1.2} \right\} \quad (36)$$

for constants  $a, b, c, d$ , where the first term models the behavior for high roughness values and the second term captures the asymptotics as  $\alpha \rightarrow 0$ .



Material	$a_n$	$b_n$	$c_n$	$d_n$	$a_m$	$b_m$	$c_m$	$d_m$
Cond.	35.275	14.136	29.287	1.8765	39.814	88.992	-98.998	39.261
Diel. (1.1)	256.47	-73.180	99.807	37.383	110.782	57.576	94.725	14.001
Diel. (1.3)	100.264	28.187	64.425	14.850	45.809	17.785	-7.8543	12.892
Diel. (1.5)	74.176	27.470	42.454	9.6437	31.700	44.896	-45.016	19.643
Diel. (1.7)	80.098	17.016	50.656	7.2798	46.549	58.592	-73.585	25.473

**Table 2:** Coefficients for the parameter heuristic defined in Equation (36).

Table 2 lists the necessary constants for boundaries of conductors and dielectrics with various indices of refraction. For indices of refraction between rows of this table, we evaluate (36) for the adjacent rows and use the bigger value.

For the Henyey-Greenstein model we use the following bound:

$$m = \frac{5.4}{1 - g} - 1.3$$

$$n = \frac{8.6}{1 - g} - 0.2$$

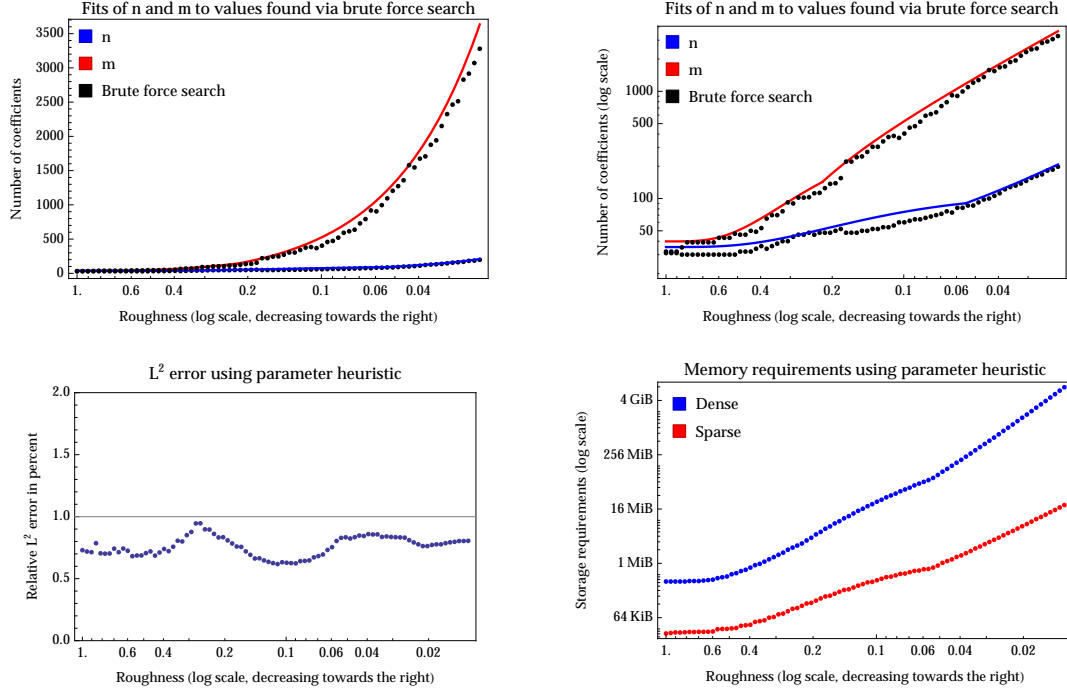
and for the von Mises–Fisher phase function we reuse the bound with  $g = \coth \kappa - \frac{1}{\kappa}$ .

## 6 Evaluation and sampling

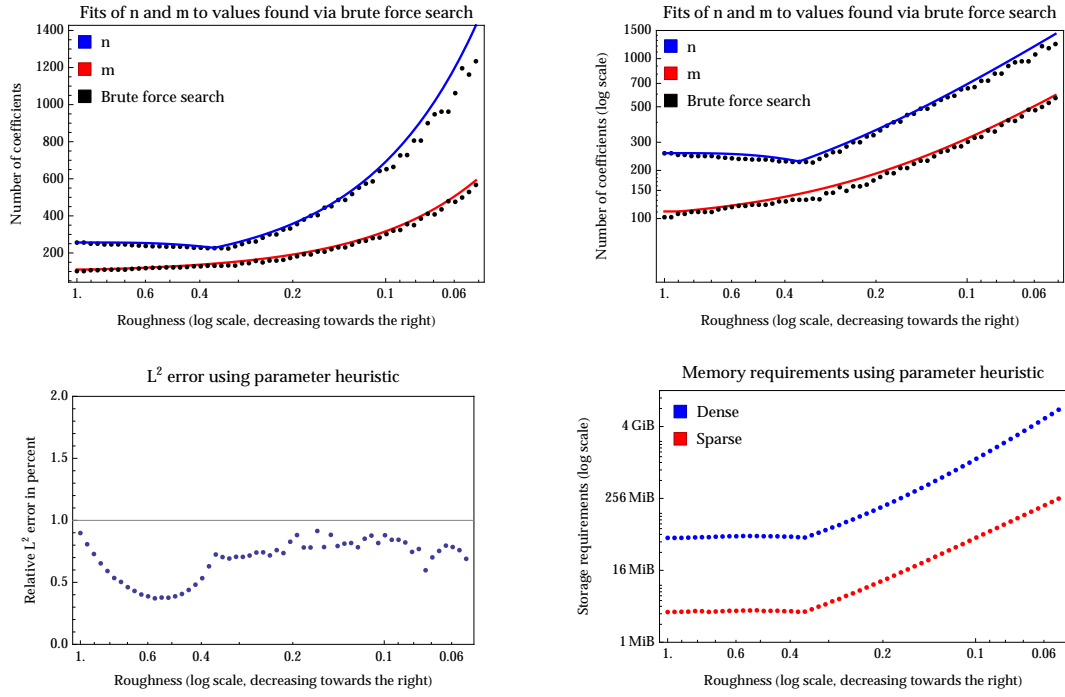
All elements of our system described until now tie into Algorithm 1 in one way or another. This algorithm runs as an offline process prior to rendering and produces a sequence of scattering matrices  $\mathbf{R}_l^t, \mathbf{R}_l^b, \mathbf{T}_l^{tb}, \mathbf{T}_l^{bt}$  ( $l = 0, \dots, m$ ). The last part of this pipeline is discussed below; its purpose is to convert the resulting data into a format that is more convenient for rendering before writing it to disk.

Recall Equation (16), which we previously used to turn a projected BSDF model  $\mathbf{F}_l$  into scattering matrices suitable for computations involving the adding equations. We now apply this equation once more in the reverse direction to convert the final set of matrices  $\mathbf{R}_l^t, \mathbf{R}_l^b, \mathbf{T}_l^{tb}, \mathbf{T}_l^{bt}$  back into a projected BSDF  $\mathbf{F}_l$  ( $l = 0, \dots, m$ ). We then transpose this tensor so that the Fourier coefficients  $(\mathbf{F}_l)_{i,j}$  are contiguous with respect to the index  $l$ , matching the order in which they will be accessed sequentially later on. To exploit sparsity, we also determine a minimal effective expansion order  $m(i, j)$  separately for each pair of elevation angles, satisfying  $(\mathbf{F}_l)_{i,j} = 0$  for  $l > m(i, j)$ . Only coefficients up to this order are stored.

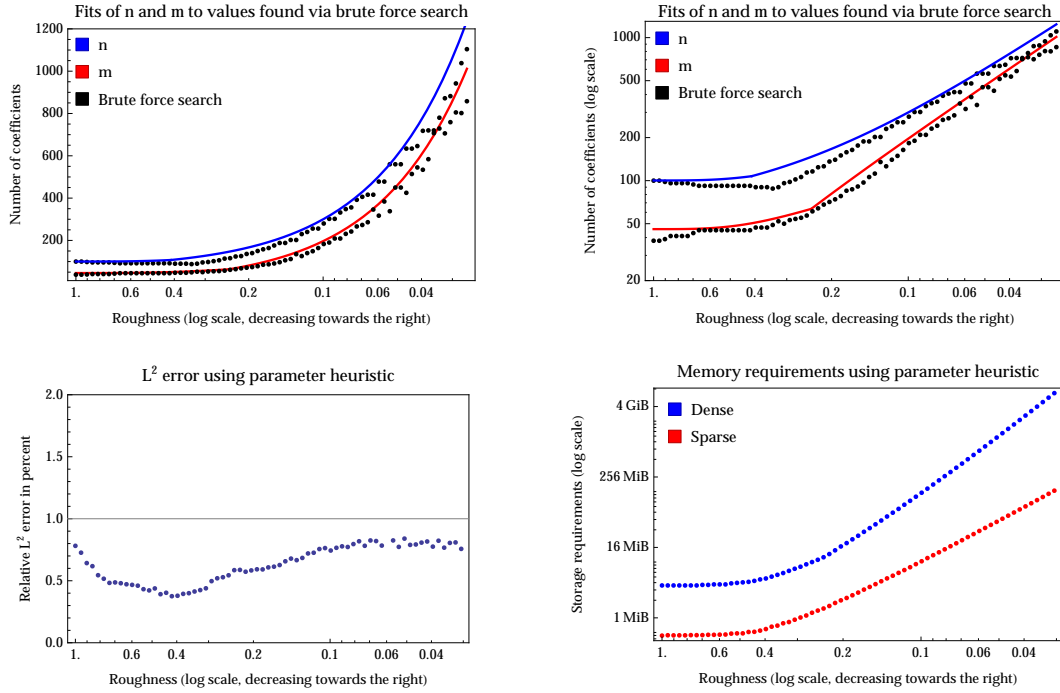
Our system handles colored materials using separate  $\mathbf{F}_l$  matrices for each color channel. In this case, we also precompute a luminance-only version of the model, which we use for importance sampling outgoing direction.



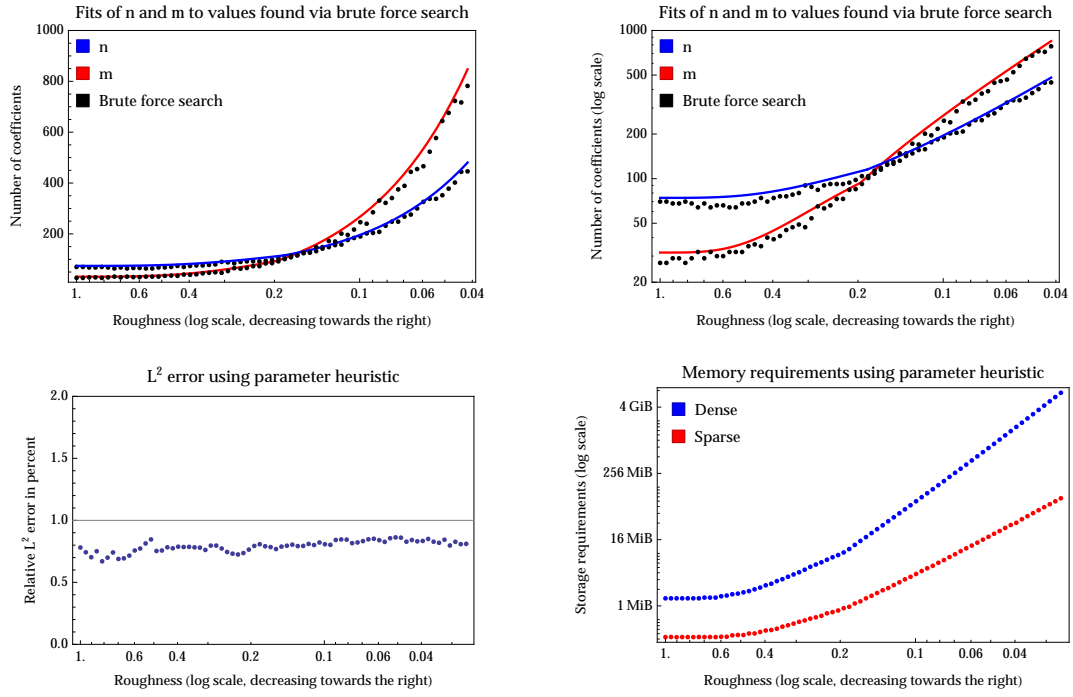
**Figure 8:** To develop a good heuristic for selecting the discretization and expansion order  $(n, m)$ , we instantiated the supported layer types of our system over a range of parameters and ran a search for the cheapest representation with less than 1% error. We bounded the resulting values from above using a simple analytic expressions that capture the asymptotics (top row: bounds in normal and log domain for a rough conductor, bottom row: storage requirements and relative error achieved by our bound).



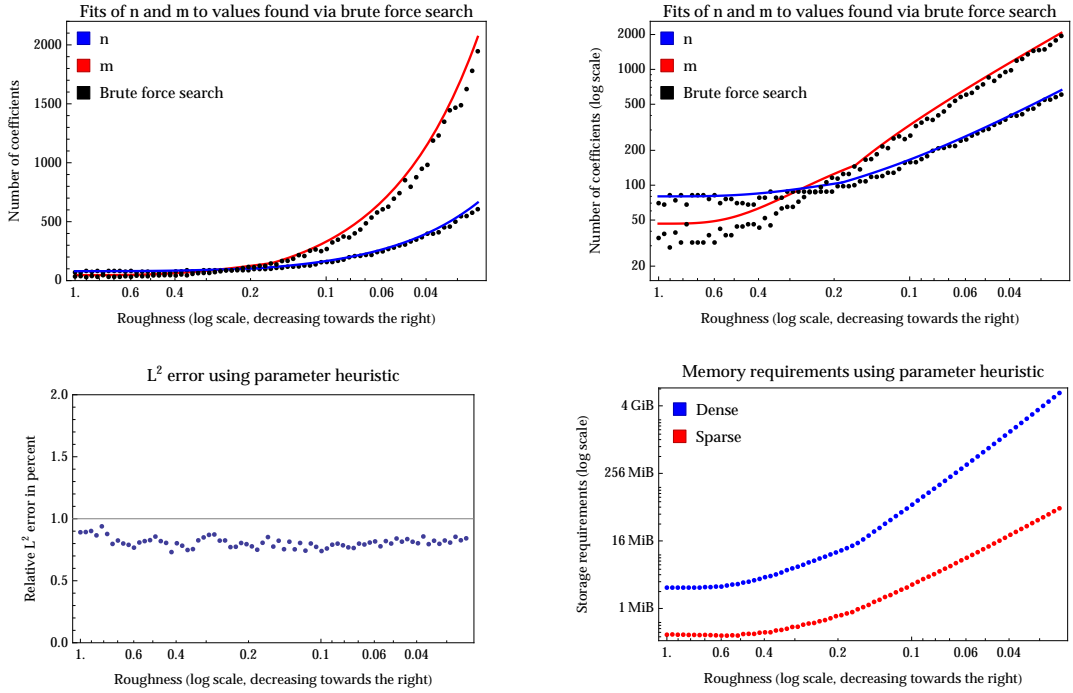
**Figure 9:** Rough dielectric ( $\eta=1.1$ ) model: parameter heuristic and error/storage analysis



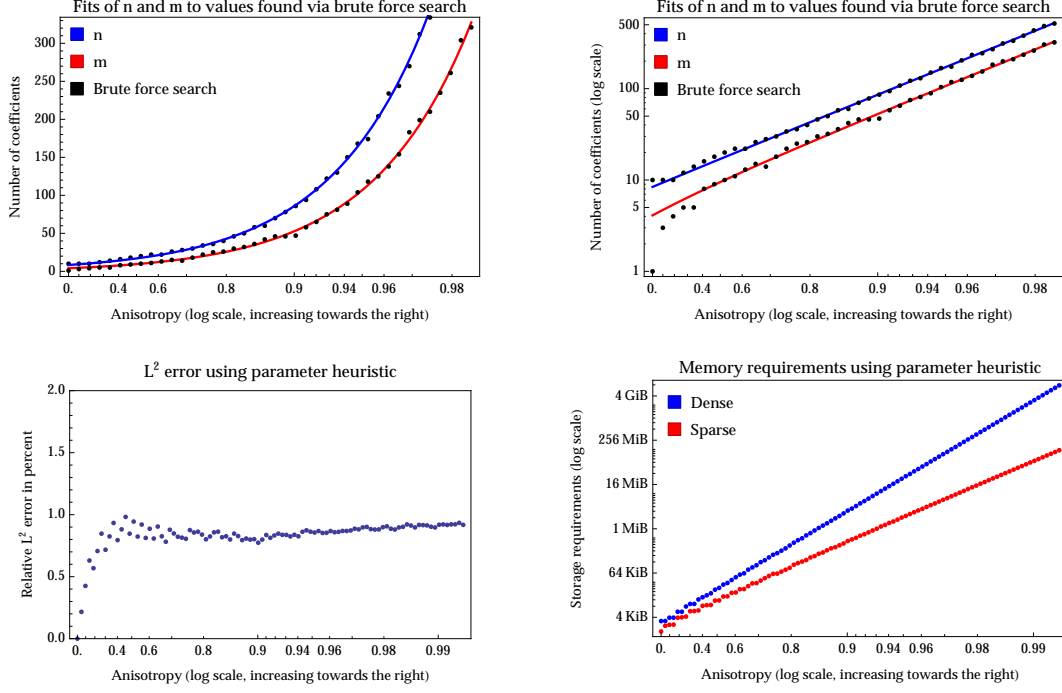
**Figure 10:** Rough dielectric ( $\eta=1.3$ ) model: parameter heuristic and error/storage analysis



**Figure 11:** Rough dielectric ( $\eta=1.5$ ) model: parameter heuristic and error/storage analysis



**Figure 12:** Rough dielectric ( $\eta=1.7$ ) model: parameter heuristic and error/storage analysis



**Figure 13:** Henyey-Greenstein model: parameter heuristic and error/storage analysis

The remainder of this section discusses how to use this information in a rendering algorithm. In our experiments, we used a standard Monte Carlo path tracer, which requires the ability to evaluate the BSDF and importance sample directions proportional to it; we show how to implement both of these operations efficiently.

## 6.1 Model evaluation

To evaluate the model for a pair of directions  $\mu_i, \phi_i$  and  $\mu_o, \phi_o$ , we determine the location in the sparse file that contains the azimuthal Fourier expansion for the given elevations ( $\mu_i, \mu_o$ ) and fetch the associated coefficients  $a_0, \dots, a_k$ . The BRDF value is then simply

$$f(\mu_i, \phi_i, \mu_o, \phi_o) = \sum_{l=0}^k a_l \cos(l(\phi_i - \phi_o)). \quad (37)$$

This works when  $\mu_i$  and  $\mu_o$  are part of the set of discretized elevations, but this is generally not the case. For intermediate values, we interpolate the Fourier coefficients from those of nearby elevation angles on the fly using the  $4 \times 4$  interpolation stencil of a standard 2D tensor product Catmull-Rom spline.

A naïve implementation of Equation (37) can lead to serious performance issues during rendering due to very many trigonometric function calls per BSDF evaluation.

To reduce these to a minimum, we use the multiple angle formula for cosines

$$\cos(n\phi) = 2 \cos(\phi) \cos((n-1)\phi) - \cos((n-2)\phi) \quad (38)$$

as a recurrence while iterating through the terms of the sum. To accelerate computations even further, we exploit instruction level parallelism when evaluating (37). All sum terms are independent from each other, and hence we can load and process groups of several coefficients at a time, using iterated forms of (38) to find the cosine values needed for the entire group in one step.

**Texturing:** To texture an arbitrary parameter of a layer (e.g. its optical depth  $\sigma_t$ ), we compute several BSDF models corresponding to samples throughout the targeted parameter domain. To evaluate the BSDF for a particular parameter value we simply interpolate between these models. For parameters with a linear dependence, two samples suffice; higher numbers are necessary to capture nonlinear effects. Multiple parameters can be textured simultaneously, though eventually the exponential growth in the required number of samples becomes burdensome. This scheme is approximate but works very well in practice for many types of parameters, including diffuse or phase function albedos or optical depth. Other parameters are less suitable (e.g. index of refraction and boundary roughness) and may require many samples when textured in this way. This is a limitation of our system and an interesting avenue for future work.

## 6.2 Importance sampling

The spline interpolation scheme introduced in Section 6.1 induces continuous extensions of the BSDF matrices  $\mathbf{F}_l$  to piecewise polynomial functions  $F_l : [-1, 1] \times [-1, 1] \rightarrow \mathbb{R}$ . For any two angles  $(\mu_i, \mu_j)$  from the initial discretization,  $F_l(\mu_i, \mu_j)$  simply returns entry  $(i, j)$  from the underlying matrix; for arguments that lie between samples of the discretization, nearby entries are interpolated.

Note the special significance of the 0-th order function  $F_0$ , which describes the average value of the BSDF integrated over azimuth:

$$F_0(\mu_i, \mu_o) = \frac{1}{\pi} \int_0^\pi f(\mu_i, \mu_o, \phi_d) d\phi_d.$$

This means that the dependence on azimuth is effectively “marginalized” out of the model, a fact which we use to build a simple and efficient importance sampling method that is split into separate elevation and azimuth angle sampling steps. Because both can be implemented as smooth mappings from a single uniform variate to an outgoing angle, they are particularly well-suited for use with certain structured point sets, such as Sobol or Halton sequences, leading to reduced variance in renderings that use them.

Both steps involve a standard numerical inversion method for integrals, which we review for completeness: to draw samples proportional to a 1-dimensional density function  $q(x) \geq 0$  on an interval  $[a, b]$ , we generate a uniform variate  $\xi$  and solve for  $x$  in  $Q(x) = \xi$ , where  $Q(x) = \int_a^x q(x') dx'$ . Note that  $Q$  is continuous and monotonically increasing; since  $Q(a) = 0$  and  $Q(b) = 1$ , this guarantees that a unique solution exists;  $[a, b]$  is known as a bracketing interval. We rely on a hybrid Newton-Bisection method to invert  $Q$ , which maintains a bracketing interval as an invariant, while using Newton-Raphson steps whenever possible to benefit from quadratic convergence rates near the solution.

**Elevation sampling:** Given a fixed incident elevation  $\mu_i$ , this step picks an outgoing elevation with a probability proportional to the piecewise cubic spline function  $F_0(\mu_i, \cdot)$ . For simplicity, let us briefly assume that  $\mu_i$  is equal to one of the elevation angles from the discretization. Let  $I_{i,k}$  denote the definite integral of  $F_0(\mu_i, \cdot)$  up to the  $k$ -th spline segment, i.e.

$$I_{i,k} := \int_{\mu_1}^{\mu_k} F_0(\mu_i, \mu') d\mu' \quad (k = 1, \dots, n).$$

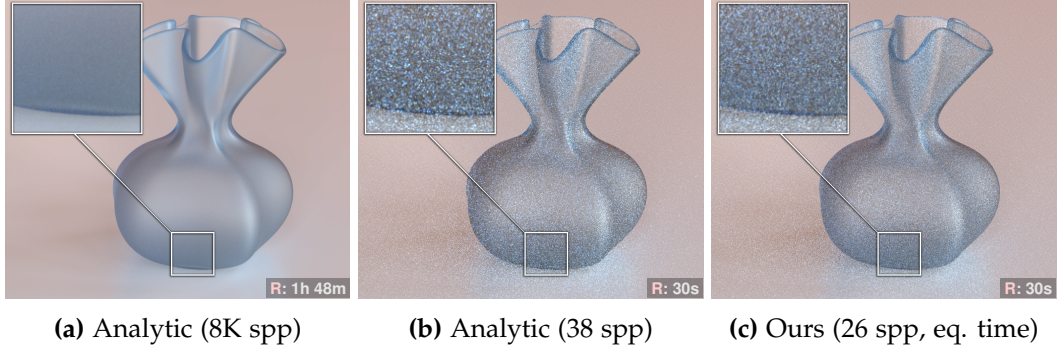
We first use a  $\mathcal{O}(\log n)$  binary search to map a uniform variate  $\xi_1 \in [0, 1)$  to the segment  $k$  satisfying  $I_{i,k} \leq \xi_1 I_{i,n} < I_{i,k+1}$ . Following this, we apply the discussed Newton-Bisection method to robustly invert the integral of  $F_0$  (a quartic) on  $[\mu_k, \mu_{k+1}]$ , producing the desired outgoing elevation  $\mu_o$ . The entries of the matrix  $I_{i,k}$  have analytic solutions that can be precomputed ahead of time. Elevations  $\mu_i$  that lie between samples of the discretization are easy to handle due to the linearity of this setup: we can simply interpolate the precomputed integrals  $I_{i,k}$  using the same Catmull-Rom basis.

**Azimuth sampling:** To sample the azimuthal component conditioned on  $(\mu_i, \mu_o)$ , we fetch the associated interpolated Fourier coefficients  $a_l := F_l(\mu_i, \mu_o)$  from the sparse coefficient storage and pick an azimuth difference angle  $\phi_d$  proportional to the resulting Fourier expansion  $q(\phi_d)$ . Finally, we set  $\phi_o = \phi_i + \phi_d$ . As before, the main sampling operation involves the inversion of a definite integral  $Q$  using the hybrid Newton-Bisection approach. This integral fortunately has a simple explicit form:

$$Q(\phi_d) = \int_0^{\phi_d} \sum_{l=0}^m a_l \cos(l\phi'_d) d\phi'_d = a_0 \phi_d + \sum_{l=1}^m l^{-1} a_l \sin(l\phi_d)$$

The recurrence from Section 6.1 can also be applied here to avoid costly trigonometric function evaluations. Instruction level parallelism offers further acceleration opportunities.

The proposed importance sampling scheme is *exact* in the sense that it produces a constant importance weight  $\leq 1$  over all scattered directions when holding the incident



**Figure 14:** Reflectance models generated by our system support exact importance sampling, which can make them interesting even in cases where an analytic reflectance model exists. The images on the middle and right show equal-time renderings of a sand-blasted vase modeled using a standard microfacet BSDF. Note improved convergence in (c) despite the lower number of samples per pixel.

direction fixed. Additional terms (e.g. the cosine of the surface illumination integral) are easily absorbed into the data to account for them as well.

This is a rare situation, since BSDF sampling techniques are almost never exact. This effectively means that our approach can be interesting even when an analytic (and potentially faster to evaluate) reflectance model is available. Figure 14 shows a rough glass vase ( $\eta = 1.5, \alpha = 0.3$ ) rendered with the analytic evaluation and sampling of Walter et al. [2007] and the approach presented in this section. Renderings were performed using Quasi Monte-Carlo integration, specifically scrambled Halton points.

The analytic sampling technique only samples one factor of the model (the microfacet distribution) and relies on a transformation from microfacet normals to outgoing directions, which distorts the equidistribution of the Halton points. In comparison, our technique is able to sample *all* terms of the BSDF directly on the sphere of outgoing directions.

### 6.3 Harmonic extrapolation

In looking to further reduce the computation time and storage requirements of BSDFs generated by our system, we analyzed a large set of scattering and absorbing slabs with interfaces of different roughness. We found that the azimuthal dependence of the resulting reflection and transmission profiles could often be described by a simple low-dimensional family of functions.

In particular, they were closely approximated by a linear combination of a constant term and a *wrapped Gaussian* distribution on the circle, i.e.:

$$g_{\delta, \beta, \sigma^2}(\phi) := \frac{\delta}{2\pi} + \beta \sum_{k=-\infty}^{\infty} G(\phi + 2\pi k, \sigma^2),$$



where  $G(x, \sigma^2)$  is a normalized Gaussian of variance  $\sigma^2$ . To fit an existing azimuthal Fourier series  $a_0, \dots, a_m$ , we require the first three circular moments of  $g_{\delta, \beta, \sigma^2}$  to agree with the coefficients  $a_i$ . Using the property that

$$\mathcal{F}_l \left[ \sum_{i=-\infty}^{\infty} G(\phi + i2\pi, \sigma^2) \right] = \frac{1}{\pi(1 + \delta_{0l})} e^{-l^2 \sigma^2 / 2}$$

this results in the system of equations

$$\begin{aligned} a_0 &\stackrel{!}{=} \mathcal{F}_0 [g_{\delta, \beta, \sigma^2}] = (\delta + \beta) / 2\pi \\ a_1 &\stackrel{!}{=} \mathcal{F}_1 [g_{\delta, \beta, \sigma^2}] = \beta / \pi e^{-\sigma^2 / 2} \\ a_2 &\stackrel{!}{=} \mathcal{F}_2 [g_{\delta, \beta, \sigma^2}] = \beta / \pi e^{-2\sigma^2} \end{aligned}$$

which can be solved for

$$\delta = 2\pi a_0 - \frac{\pi a_1^{4/3}}{\sqrt[3]{a_2}}, \quad \beta = \frac{\pi a_1^{4/3}}{\sqrt[3]{a_2}}, \quad \sigma^2 = \log \frac{a_1^{2/3}}{a_2^{2/3}}$$

Since this approach extrapolates the entire behavior from the first three harmonics, Algorithm 1 can be stopped after  $m = 2$ , which significantly reduces the precomputation time. When evaluating the function  $g_{\delta, \beta, \gamma}$  during rendering, we use the approximation

$$\widehat{g}(\phi) = \frac{\delta}{2\pi} + \begin{cases} \sum_{i=-1}^1 G(\phi + i2\pi, \sigma^2), & \sigma^2 < 5 \\ (1 + 2 \cos(\phi) e^{-\sigma^2 / 2}) / 2\pi, & \text{otherwise} \end{cases}$$

which has maximum relative  $L^2$  error of approximately 0.005. Importance sampling this representation is trivially implemented by randomly drawing a sample from a uniform distribution or a normal distribution and taking the result modulo  $2\pi$ .

## 7 Results

We implemented this technique in C++ on top of the Mitsuba renderer [Jakob 2010], relying on the Eigen library [Guennebaud et al. 2010] for sparse linear algebra computations. BSDF sampling and evaluation exploit instruction parallelism using Intel’s AVX instruction set. To solve the sparse linear systems in the adding Equations (Section 3.1), we use supernodal LU decompositions [Li 2005].

To ensure the correctness of our system, we routinely performed validation tests—these included checking that projection of scattering models into the directional basis is accurate, comparing against reference data including angular reflectance data of index-matched isotropic and anisotropic slabs (Tables 12 and 35 of [van de Hulst 1980]) and albedo values for isotropic half-spaces with dielectric boundaries [Williams 2006].



**Figure 15:** All materials in this interior scene were generated and rendered using the techniques described in this paper. The insets on the left and right reveal the corresponding structural descriptions that were used as inputs to our system.

Material	$n$	$m$	Time	Storage	Sparsity
Coffee table	394	671	3.34s	68.4MiB	5.7%
Red vase	196	267	2.09s	11.9 MiB	9.9%
Coated copper vase	196	267	2.52s	3 MiB	2.5%
Large purple bowl	196	267	4.31s	5.2 MiB	4.3%
Measured BRDF	200	200	1.69s	22.7MiB	24%
Coated measured BRDF	200	267	3.49s	3.2 MiB	2.5%
White brick wall	196	267	0.96s	1.3 MiB	3.2%
Kitchen sink	502	890	7.52s	9.6 MiB	1.1%
Kitchen counter (wood)	394	671	6.5s	55.5 MiB	1.2%
Kitchen counter (metal)	236	4194	1.41s	10.1 MiB	0.38%

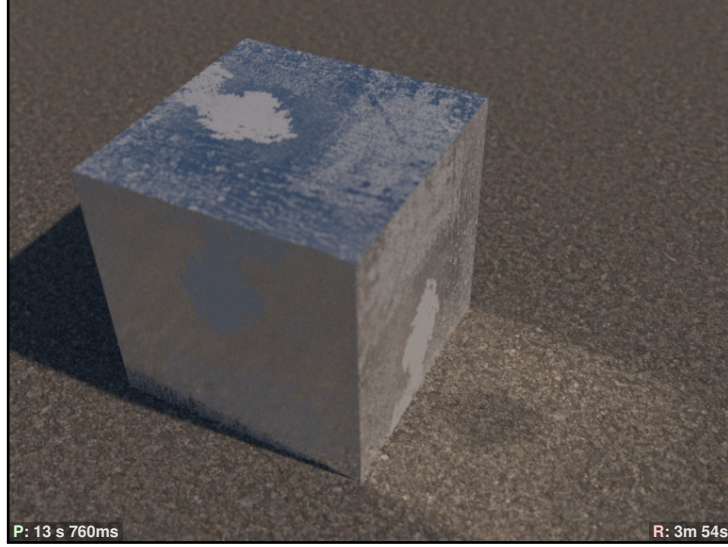
**Table 3:** Discretization, preprocessing time, storage requirements, and the percentage of nonzero coefficients of the objects in Figure 15.

Finally, we also ran comparisons against Monte Carlo renderings with explicit layer structure. In all cases, our validations showed excellent agreement, usually matching reference data in the radiative transfer literature to four significant digits.

We now present a series of results produced using our system. Precomputation and rendering times are reported for an Intel Xeon E5-2660 machine with 16 physical (32 hyper-threaded) cores.

## 7.1 Interior scene

Figure 15 depicts a range of layered materials generated by our model. The corresponding layer structures are shown on the sides, and detailed statistics regarding processing time and storage requirements are presented in Table 3. The wooden kitchen counter material is a coated diffuse surface with texture-mapped albedo; to



**Figure 16:** Gu et al. [2007] provide a database of measured surface contaminants. We use one of their optical thickness maps to render a shiny chrome cube with dried deposits due to salt water exposure. Note how the salt blocks part of the caustic on the ground.

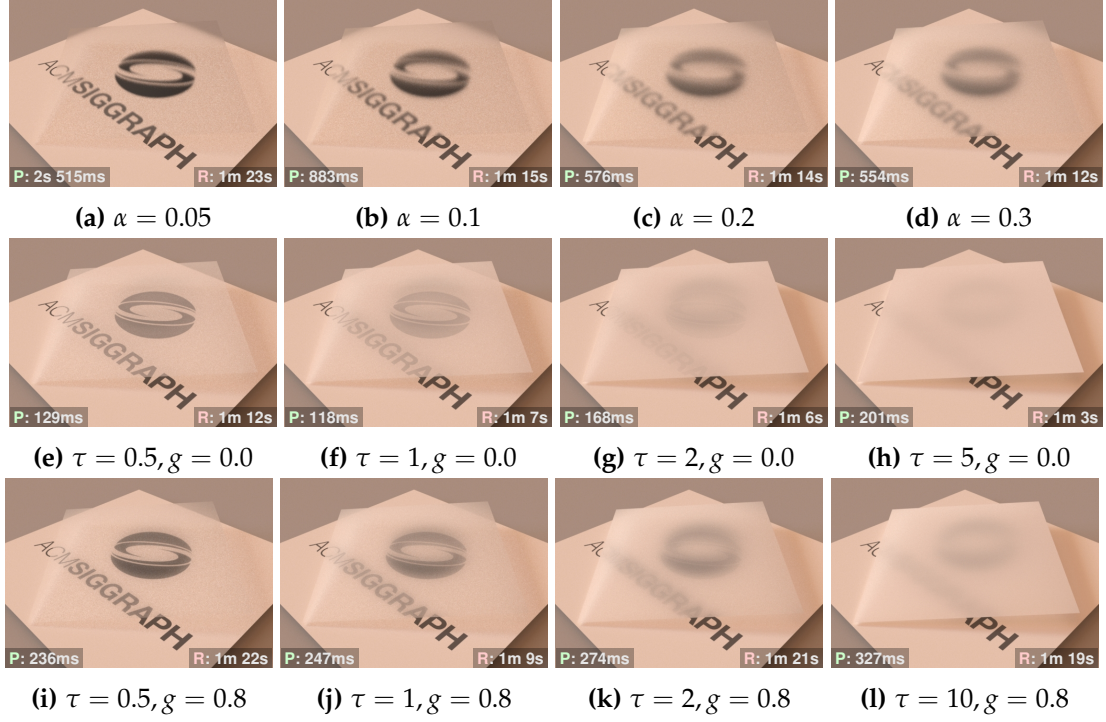
capture the material’s non-linear dependence on albedo we use four BRDF samples over the admissible parameter range  $[0, 1]$ . Following precomputation, the image was path traced at with a resolution of  $1800 \times 1080$  pixels using 2048 samples per pixel to resolve glossy interreflections between objects, which took 1 hour and 23 minutes.

## 7.2 Contaminants maps

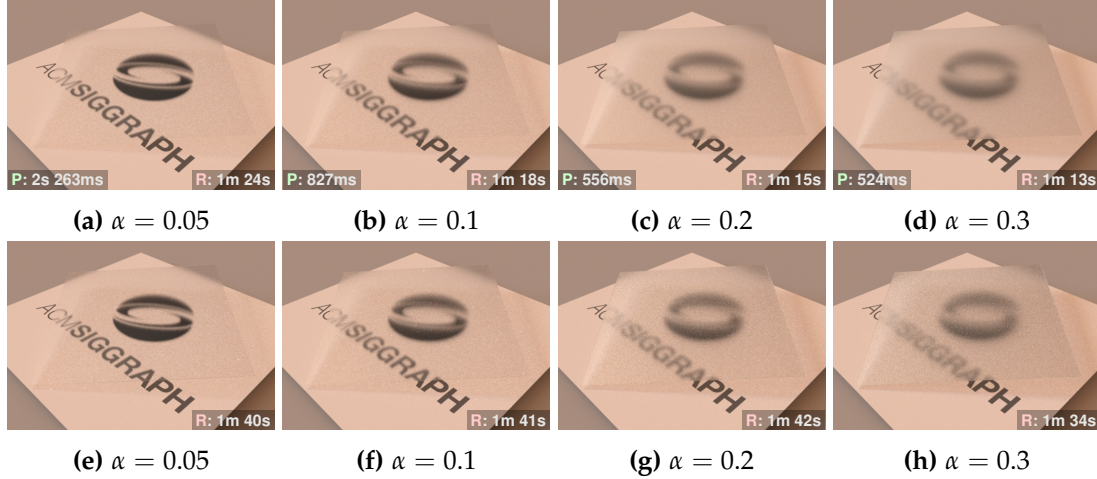
Figure 16 shows a shiny chrome cube with dried salt water deposits rendered under daylight illumination. We modeled this as a shiny chrome base ( $\alpha = 0.03$ ) with an index-matched anisotropic layer ( $g = 0.7$ ) whose optical thickness is textured by a contaminant map of Gu et al. [2007]. To capture the nonlinear dependence in  $\sigma_t$ , we precomputed six BRDF samples over the parameter range. The combined BRDF with discretization  $n = 158$  and expansion order  $m = 2540$  required 21.6 MiB as opposed to 4.3 GiB for a dense version (a reduction to 0.5%) and was computed in 13.7 s. Rendering using Manifold Exploration MLT [Jakob 2013] using 64 mutations/pixel took 3m 54s.

## 7.3 Surface vs. volumetric scattering

The two classes of transport operators in our framework—surface and volume—act on the incoming light fields in fundamentally different ways. It is instructive to analyze their behaviors in isolation. Figure 17 compares the different loss of clarity caused by



**Figure 17:** Comparing the visual loss in clarity as caused by surface roughness versus volumetric scattering inside a layer. The top row ((a)-(d)) shows the transmission through an index 1.5 dielectric plate with identical Beckmann roughness  $\alpha$  on both faces. The lower two rows demonstrate index-matched plates with volumetric imperfections simulated by HG scattering (which may be appropriate for material with air pockets or other inclusions). A variety of appearances is evident as the optical thickness and anisotropy are varied ((e)-(l)). The rough dielectric scattering produces a blurring effect, while the volumetric scattering leads to a hazing of the transmitted signal. Rendered at a resolution of  $512 \times 512$  pixels using 1024 samples per pixel.



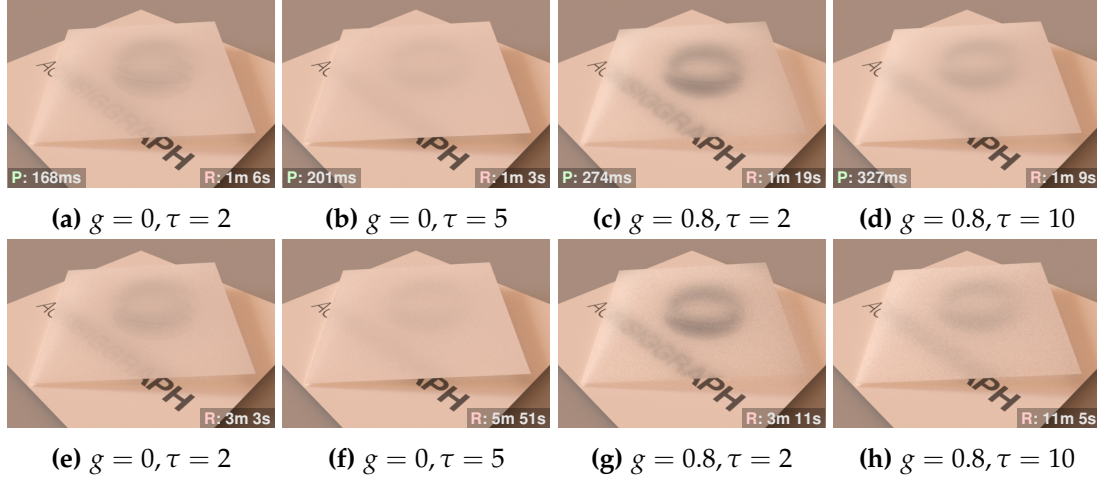
**Figure 18:** Top: our method using a single plane geometry to represent a glass plate roughened on both sides. Bottom: a reference scene with an explicit thin glass plate with a rough dielectric BSDF on both faces. Beckmann roughness  $\alpha$  is the same on both faces and varied left to right. The multiple scattering correction term is disabled in this rendering to facilitate the comparison. Note the increased variance in the bottom row, which is due to the importance sampling routine of the classical model. All images in this figure were rendered at a resolution of  $512 \times 512$  at 1024 samples per pixel.

transmission through layers with rough surfaces versus layers with smooth surfaces, but with internal volumetric scattering. Roughening both sides of the glass plate causes a uniformly blurred transmission of the background scene, whereas forward-peaked volumetric scattering inside plates with smooth surfaces causes more of a hazed appearance. The arbitrary combination of this wide variety of operators yields a very flexible system for building BSDFs.

## 7.4 Asperity Scattering and Diffuse Materials

Adding a volumetric scattering layer to a base material can be used for asperity scattering [Koenderink and Pont 2003], useful for simulating fine layers of dust or fibers on a surface. We illustrate this in Figure 20 by visualizing various forms of asperity layerings on a black base layer, and then to simulate dust on a gold statue. Note that these renderings resemble those of Pharr and Hanrahan [2000], whose nonlinear scattering equations provide an alternative way of solving for the interaction between layers. However, their approach does not lead to a reflectance model in explicit form: during the rendering process, every interaction with a layered material triggers a nested Monte Carlo integration over layers. Our system is the first to account for all orders of interreflection between an asperity and underlying layer, and to include multiple scattering in the asperity layer without requiring a costly integration over layers at





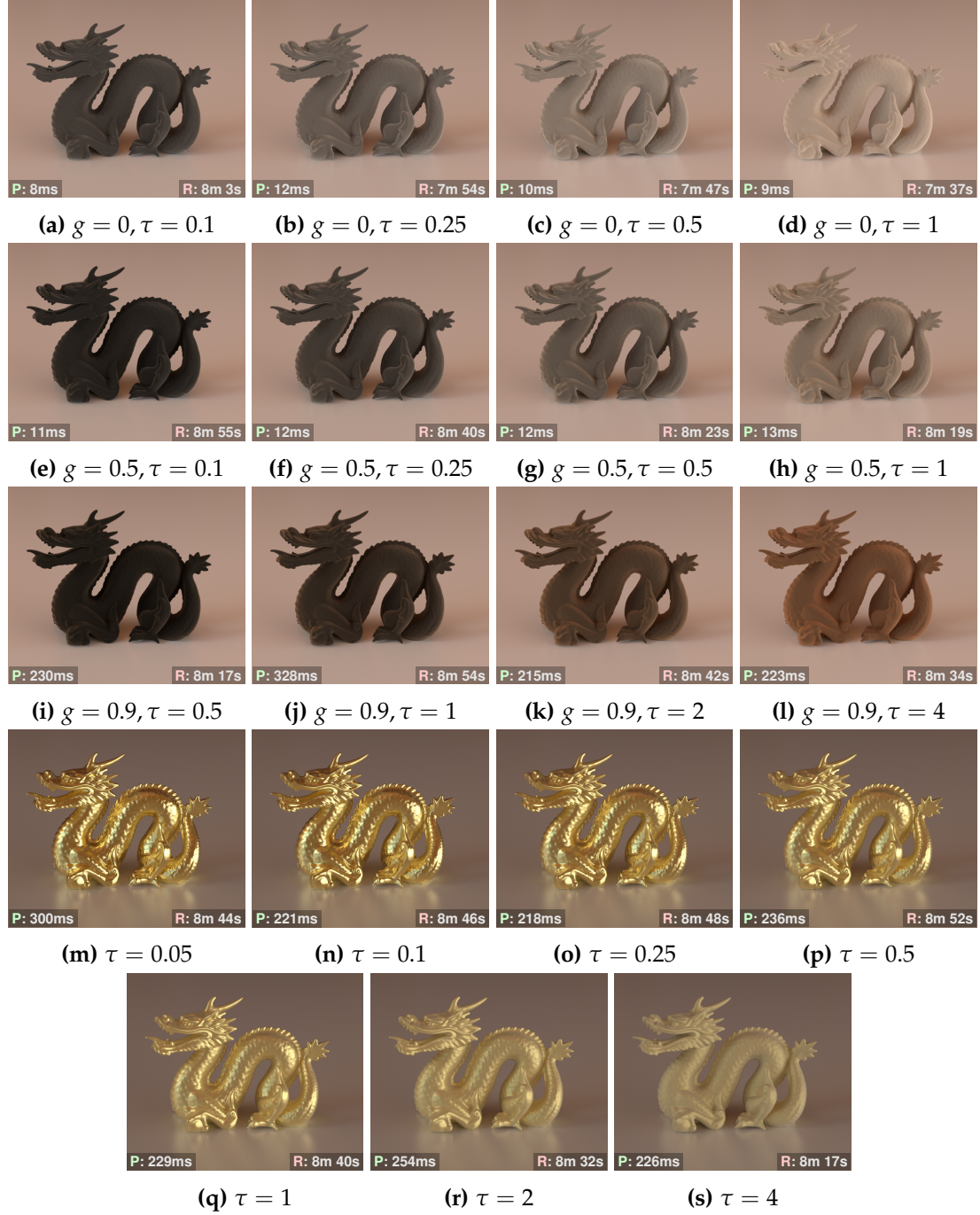
**Figure 19:** Top: our method using a single plane geometry to represent a volumetric HG-scattering layer. Bottom: a reference scene with an explicit smooth glass plate with brute force Monte Carlo scattering inside. Note the increase in rendering time for thicker layers in the Monte Carlo simulations. All images were rendered using 1024 samples per pixel.

render time.

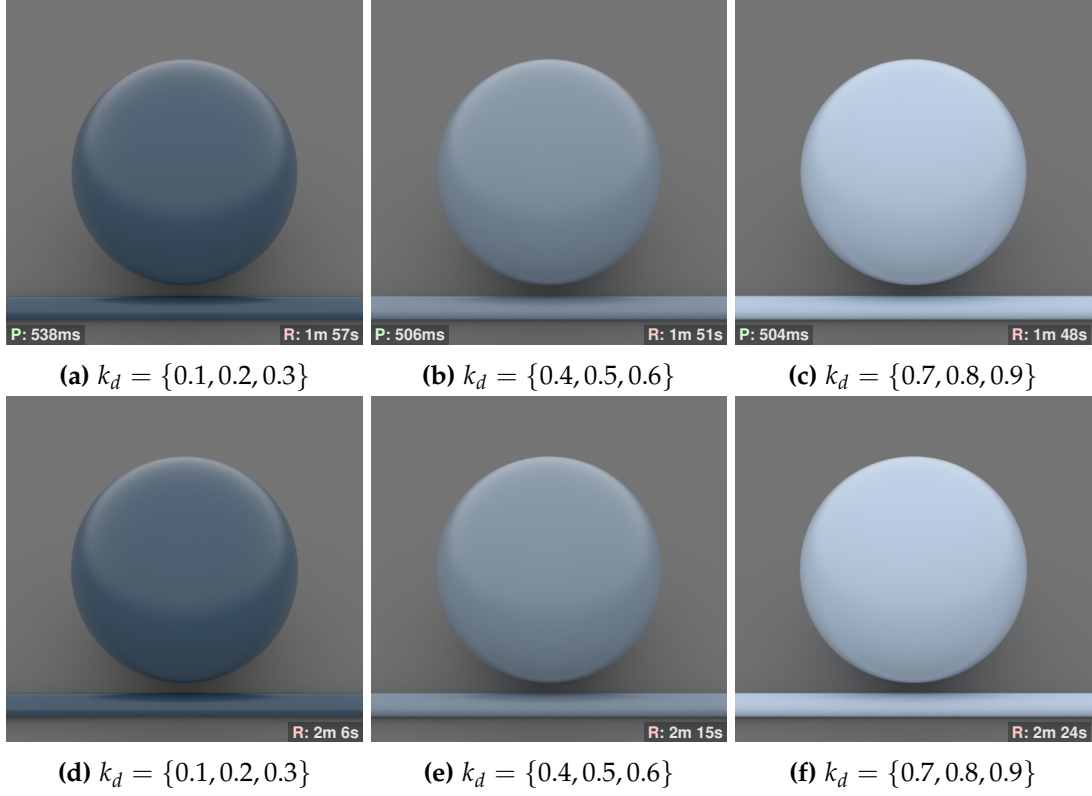
Volumetric scattering layers can yield a wide variety of new diffusive BRDFs that complement that standard analytic models. Figure 22 compares Lambert and Oren-Nayar BRDFs to volumetric scattering materials with isotropic or forward-peaked Henyey-Greenstein scattering. The use of an isotropic scattering material (c) yields a very dusty look, which is lessened in (d) by layering a HG scattering layer  $g = 0.8, \tau = 5$  on top of a 90% Lambertian reflector. The volumetric-scattering renders were no more than 30% slower, and the BSDFs were compactly stored in 3.5 KiB.

## 7.5 Approximate layered BRDFs

The model of Weidlich and Wilkie [2007] supports texturable layered materials with anisotropic interfaces but does not account for all orders of interreflection between layers. This leads to incorrect albedos from simple combinations, such as a smooth dielectric interface over a Lambertian reflector. Figure 23 compares the total albedo of such a model with refractive index 1.5 as a function of diffuse reflectance  $k_d$  of the underlying Lambertian surface. Due to internal scattering, the total reflected energy has an inherently nonlinear dependence on  $k_d$ . Weidlich and Wilkie’s model discards such internal reflection light paths and uses an heuristic scaling factor to compensate for the resulting loss of energy. However, the nonlinear behavior of the layers is not captured regardless of whether or not the heuristic is used. Another limitation of this approach is that it cannot faithfully simulate the interaction of multiple rough

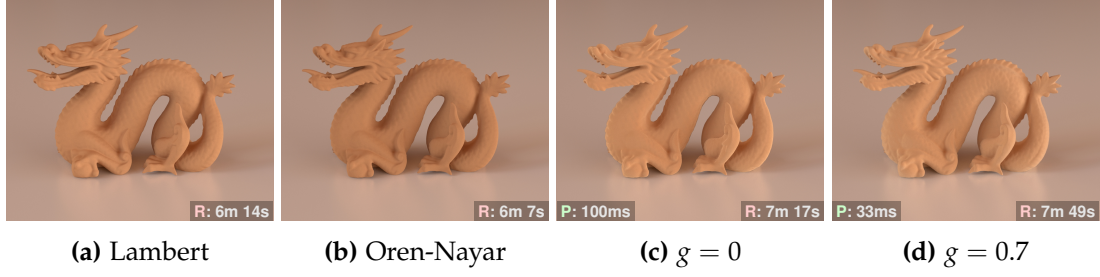


**Figure 20:** Top: asperity scattering using a volumetric scattering layer on top of a black surface. Various thicknesses  $\tau$  and HG phase functions (with mean cosine  $g$ ) are compared. The single-scattering albedo is slightly orange in all cases. Because more scattering events are required to scatter a similar amount of light for  $g = 0.9$  as for the isotropic case (using much larger optical thickness), the result is more saturated. Bottom: applying various thicknesses  $\tau$  of grey HG ( $g = 0.9$ ) dust to a rough gold statue. All images were rendered at a resolution of  $1200 \times 1000$  pixels using 1024 samples per pixel.



**Figure 21:** Here we compare (top row) our BRDF for a rough Beckmann dielectric interface ( $\alpha = 0.1$ ,  $\eta = 1.5$ ) over top of a Lambertian base layer with various (RGB) values of diffuse reflectance  $k_d$ . The bottom row shows a brute force simulation with a slightly larger rough dielectric sphere surrounding an interior Lambertian sphere. The adding equations in our approach account for all orders of interreflection between the two layers, producing accurate total albedos. The images in both rows were rendered at a resolution of 1024x1024 pixels using 512 samples per pixel and slightly cropped.





**Figure 22:** A wide variety of diffusive reflectance models are possible by combining volumetric scattering layers and Lambertian reflectors. Note the different silhouettes and overall subtle appearance differences between the volumetric models in (c) and (d) vs. the traditional diffuse BRDFs in (a) and (b). Both (a) and (b) have spectral albedos  $k_d = \{0.5, 0.25, 0.12\}$ , with the Oren-Nayar render using a roughness  $\alpha = 0.6$ . For (c) and (d) spectral single-scattering albedos  $a$  were selected so as to produce diffuse albedos of  $\{0.5, 0.25, 0.12\}$  under normal incident illumination. For (c) with isotropic scattering,  $a = \{0.938, 0.759, 0.513\}$ . For (d),  $a = \{0.983, 0.93, 0.833\}$ . The images above were rendered at a resolution of  $1200 \times 1000$  pixels using 1024 samples per pixel.

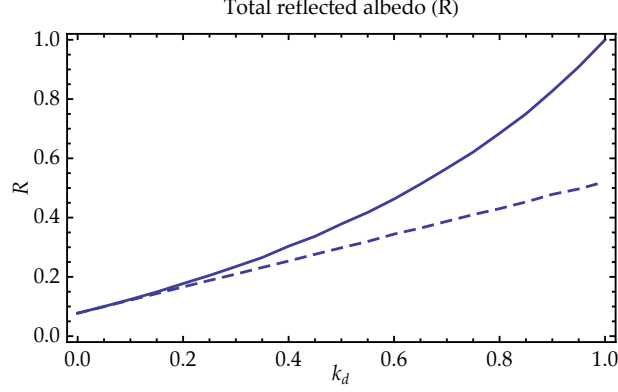
boundaries, which requires a full integration over internal reflection paths.

## 7.6 Fitting to measured data

We also conducted measurements of real-world materials with the goal of reproducing observed reflectance curves using our model. Our experiments focused on vitreous enamel coatings used in traditional jewelry design. Such enamels are usually available in powdered form and consist of lead glass colored by cobalt compounds or similar pigments (Figure 24 (a)). To coat an object, the enamel powder is mixed with water to turn it into a thick paste, which is then applied to the object using a paintbrush and dried. Finally, the object is heated to a temperature around  $830^\circ\text{C}$ , causing the powder to melt and turn into a homogeneous glaze under the influence of surface tension.

To conduct reflection and transmission measurements of enamel layers, we prepared 1 mm thick swatches of fine silver with a punched-out circular hole of 8 mm diameter that was filled with enamel of the same thickness (i.e. 1 mm, see Figure 24 (b)). We did this by laser-welding a smooth sheet of metal<sup>1</sup> foil onto one side of the swatch to firmly close the circular hole. Next, we filled the resulting cavity with enamel paste and melted it in a furnace, making sure to use enough enamel so that the solidified enamel protrudes out of the cavity. After grinding down the protrusion and a second melting pass, the metal foil on the bottom can be peeled off to yield a 1 mm thick layer of enamel with a smooth finish on both sides; this type of enamel preparation is also

<sup>1</sup>We used gold foil to prevent chemical reactions between the enamel surface and the foil at melting time, which can lead to slight color shifts.



**Figure 23:** Comparing the total reflected energy  $R$  of a smooth dielectric  $\eta = 1.5$  on top of a Lambertian surface with reflectance  $k_d$ . A recent approximate model (dashed) proposes a linear relation between  $k_d$  and total reflectance, which is not seen in the exact solution that considers all orders of interreflection.

known as *plique-à-jour*.

We mounted the resulting swatches at the center of a spherical gantry. In our setup (Figure 25), a stationary DSLR camera (Canon EOS 50D) measured the radiance leaving the surface along the normal direction, while a rectangular area light source performed a  $180^\circ$  sweep around the sample. For light each angle, we took an exposure series and merged it into a HDR image. The black dots in Figure 26 show transmission and reflectance measurements for a milky light blue enamel swatch. The angle  $\theta = -90^\circ$  on the horizontal axis corresponds to the camera and light source being exactly opposite to each other and normal to the swatch. We did not record results for angles  $|\theta| < 30$  and  $\theta > 70$  due to occlusion by the sample holder and camera, respectively.

We replicated this lighting and viewing geometry in our simulation framework and performed an automated search for a layer that best fits the observed data. The enamel swatch was modeled as a rough dielectric slab filled with a Henyey-Greenstein medium. Our enamels had 38% lead (II) oxide content, giving them an index of refraction of approximately 1.586, and we manually estimated the roughness of the interfaces to be around  $\alpha \approx 0.05$ . This left a three parameter family of models to be searched involving the single scattering albedo, extinction, and anisotropy. The search was greatly accelerated using the following observations:

1. The simulated radiance measurement corresponding to the  $\theta = -90^\circ$  transmission configuration decreases monotonically when increasing the extinction  $\sigma_t$ . A simple bisection search can thus be used to select  $\sigma_t$  such that the simulated data point matches the measurement (assuming that the other parameters are fixed). This bisection constitutes the innermost loop of our search procedure.



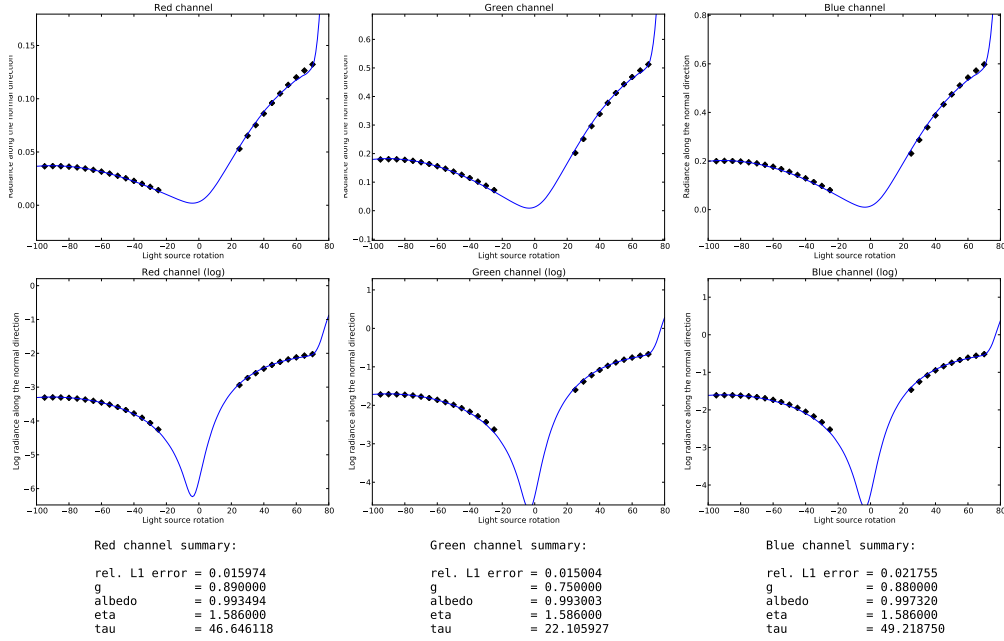
(a) A sample of jewelry enamels in powdered form

(b) Enamel test swatch

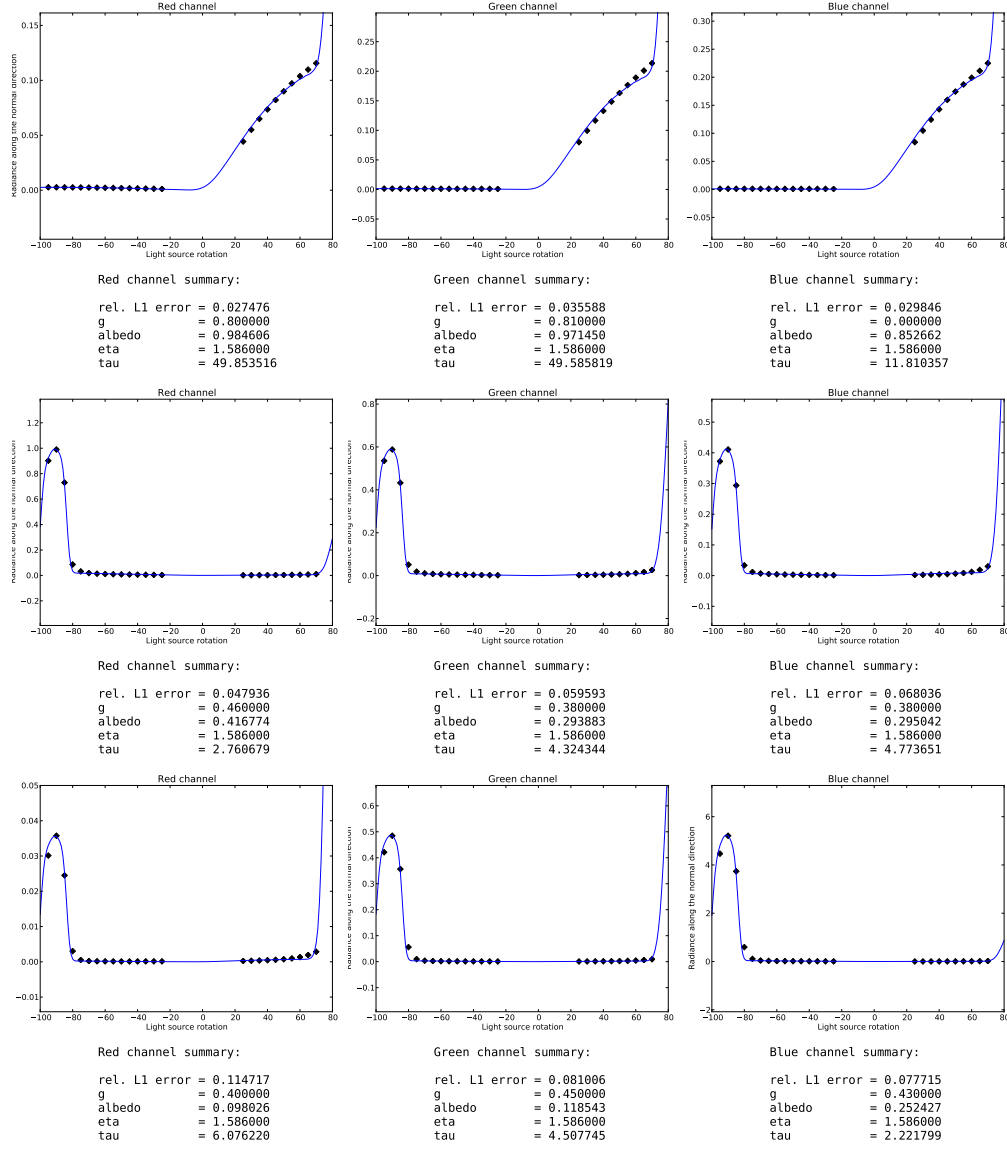
**Figure 24:** Jewelry enamels come in a wide variety of colors and range from fully absorptive to highly scattering. To acquire model parameters, we prepared 1 mm thick enamel test swatches suitable for reflectance and transmission measurements.



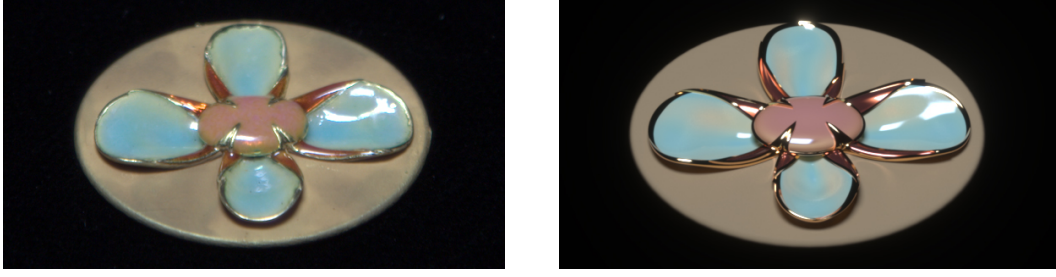
**Figure 25:** Photograph of our measurement setup: a small swatch of enamel mounted at the center of a spherical gantry is illuminated by a rotating rectangular light source, while the camera measures the radiance along the normal direction



**Figure 26:** Our method can be used to determine suitable scattering parameters for measured materials; here we fitted it to transmission and reflectance measurements of a 1 mm layer of a milky light blue vitreous enamel used in jewelry design. This dielectric had a known index of refraction and was very smooth, leaving only a three parameter family of models to be explored involving albedo, extinction, and anisotropy. An automatic search found the fit shown as a blue curve, which is in good agreement with the data (left to right: RGB, top: radiance, bottom: log radiance). Positions on the horizontal axis correspond to different light source rotations (left half: transmission, right half: reflection). The sharp increase near  $\theta = 90^\circ$  is due to specular reflection of the light source.



**Figure 27:** Measurement results for three additional jewelry enamels (from top to bottom): scattering milky red, absorbing cobalt red, absorbing cobalt blue.



**Figure 28:** Left: photograph of a flower art piece manufactured by casting a 3D printed wax model into gold and manually coating it with jewelry enamel. The petals use the same enamel also measured in Figure 26. Note the subtle hue shifts due to varying layer thickness. Right: a rendering using our framework.

2. The sum of all reflectance ( $\theta > 0$ ) measurement data points satisfies a similar monotonic relationship with respect to the single scattering albedo parameter. We also use a similar bisection search in this parameter to ensure that the sum of reflectance measurements in the simulation matches that of the real measurement. This constitutes the middle loop of the search procedure.
3. The behavior of the anisotropy parameter is more involved. In the outermost loop, we therefore perform an exhaustive search from  $g = -0.99$  to  $g = 0.99$  in increments of 0.01.

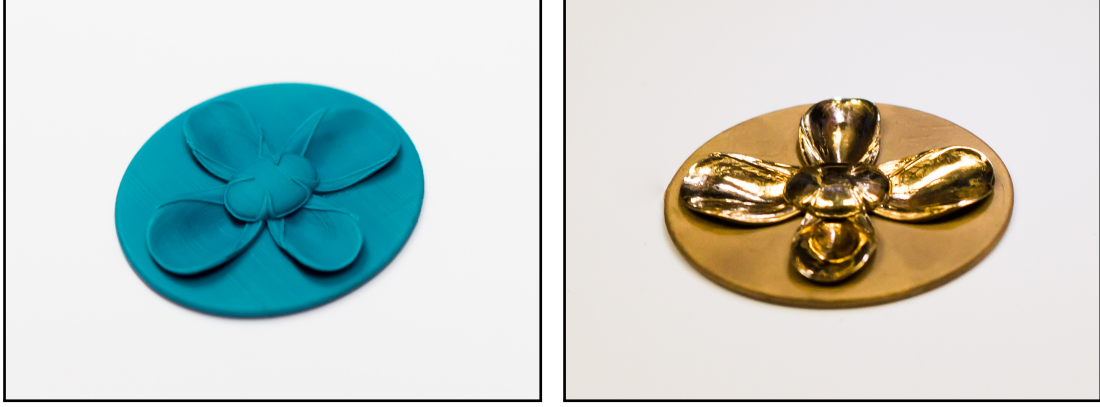
For every triplet of considered parameters, we ran a virtual measurement of a layer with the same lighting and viewing configuration and computed the  $L^1$  difference with respect to the real measurement, keeping track of the best-scoring set of parameters. Figures 26 and 27 show the results obtained in this way. Note that all parameters are given in the camera’s native color space to prevent gamut issues.

## 7.7 Applications of measured enamel parameters; predictive rendering

Being able to describe a material or coating in our framework leads to interesting possibilities, which we demonstrate on a flower art piece. This object (shown in Figure 28) was manufactured by 3D printing a triangle mesh using an industrial hard wax (Figure 29 (a)). The resulting wax object was cast into 24k fine gold using a traditional lost-wax casting process and polished (Figure 29 (b)). The gold surface was coated using the scattering red and blue and absorbing red enamels previously measured.

Since we previously acquired scattering parameters of these enamels, it should be possible to obtain a similar image by applying the coatings on top of a gold base layer within our framework and assigning the resulting BRDF models to the different parts of the triangle mesh. This is shown on the right side of Figure 28. Note that this technically not a predictive rendering, since we still had to manually set several parameters to match the photograph; in particular: the roughness of the gold base and





(a) 3D printed wax object

(b) Gold cast prior to enamel application

**Figure 29:** Intermediate steps while manufacturing the flower art piece in Figure 28.

coating, as well as the layer thickness. To simulate the effects of gravity, we defined the layer thickness as a procedural texture that depends on the surface normal  $\mathbf{n}$ :

$$T(\mathbf{n}) = c_0(c_1 + (1 - c_1)|\mathbf{g} \cdot \mathbf{n}|^{c_2})$$

where  $c_0, c_2, c_3$  are suitable constants and  $\mathbf{n}$  is the gravity vector.

Disregarding obvious differences in geometry that are due to the manual casting and enamel application, we find that our model can faithfully capture the important effects, including subtle color shifts due to variation in layer thickness.

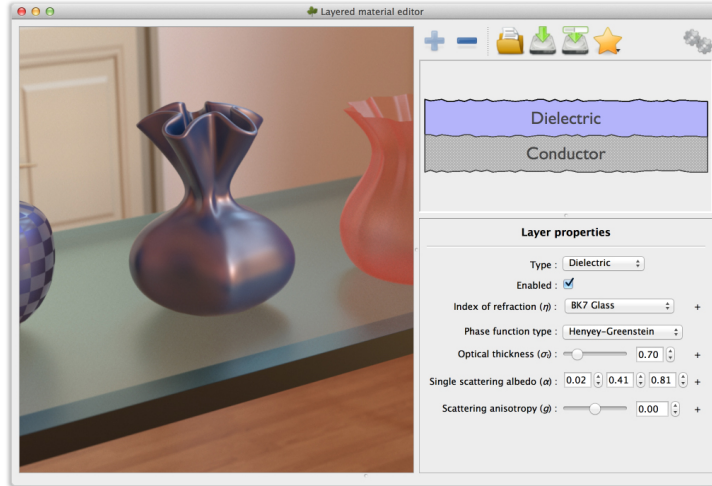
We expect that more accurate predictions of the fine-scale geometry may be available when using a carefully controlled industrial manufacturing process. Given such data and estimates of roughness and layer thickness, our model could also be used for truly predictive renderings with novel layer configurations.

## 7.8 Visual layer design tool

To conveniently assemble materials from layers and render them, we developed a visual design tool shown in Figure 30. The supplementary video contains a screen recording of an interactive material editing session using this tool.

## 8 Conclusion

We have presented a new framework for rendering layered materials. Our system allows arbitrary layered combinations of any known analytic or measured isotropic BSDF and produces new energy-conserving, reciprocal BSDFs with importance sampling. All interreflections between layers are computed at the same level of accuracy that is used for the primary light transport throughout the scene. This allows seamless



**Figure 30:** We developed an interactive visual design tool to explore the space of layered BRDF models; the supplementary video shows an editing session using it.

level-of-detail transitions for practically authoring complex scenes as well as allowing design of layered materials in a fashion that is closely tied to their physical constituents, which is useful for rapid authoring of heterogeneous or temporally-varying materials and essential for predictive rendering. Combining smooth and rough interface BSDFs with volumetric scattering layers produces a large variety of new layered BSDFs, including expressive generalizations of diffuse surfaces and asperity scattering layers. We have demonstrated the practicality of our approach, which hinges critically on novel methods for treating rough surfaces and scattering events in a stable fashion, a new method for conserving energy at rough interfaces, and also sparse methods and extrapolation techniques for compact storage and accelerated computation of our BSDFs. Our system remains practical over a large range of model parameters, scaling even to narrowly peaked reflectance functions, but cannot represent perfect mirrors or ideally smooth glass, which are Dirac delta functions in direction. Ultimately, analytic solutions exist for such cases that will be preferable to numerical approaches like ours.

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